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STRUCTURAL CALCULATIONS

Stainless Cable Solutions Merged



Prepared for: Stainless Cable Solutions, LLC. 15806 SE 114th Ave Clackamas, OR 97015

> October 21, 2020 20184



SUBJECT: Aluminum Calcs

DATE: DESIGN: PAGE:

10/20/2020

Scope of Work

Development and design for an aluminum cable railing system including:

Termination post, intermediate post, top rail, rail connecting blocks, cables, end cap, flat infill, base plate, stair facia, stair intermeadiate cap, and attachments.

General

The enclosed calculations were intended to be to designed and submitted in conformance with the following:

Professional Engineer Seals

State of Washington

State of Oregon

State of California

Building Codes (Meets or Exceeds Requirements)

2018 International Building and Residential Codes

Compliant with 2019 Oregon Structural Specialty Code and 2019 California Building Code

Additional Design References

2015 Aluminum Design Manual

2014 Building Code Requirements for Structural Concrete (ACI318-14)

AISC Steel Construction Manual, 14th Edition

2018 National Design Specification for Wood Construction

ICC Report AC273: Acceptance Criteria for Handrails and Guards

Materials			
6061-T6, T6510, T6511 Extrusions	Tensile Ultimate Strength,	Ftu =	38 ksi
	Tensile Yield Strength,	$F_{ty} =$	35 ksi
	Compressive Yield Strength,	F _{cy} =	35 ksi
	Tensile Ultimate Strength at Weld Zone,	Ftuw =	24 ksi
A554 Stainless Steel Grade 304/304L	Yield Stress,	F _y =	30 ksi
	Tensile Stress,	$F_{U} =$	75 ksi
Stainless Steel 18-8 Self Tapping Screws	Yield Stress,	F _y =	20 ksi
	Tensile Stress,	F _U =	65 ksi
Type 316 Stainless Steel Wire Rope	1x19 Strand Core		
	1/8" dia. with breakir	ng strength =	1869 lbs
	7x7 Strand Core		
	1/8" dia. with breakir	ng strength =	1566 lbs
Weld Filler Material 4043	Tensile Ultimate Strength,	Ftuw =	24 ksi



SUBJECT: Aluminum Calcs

DATE: DESIGN: PAGE:

10/20/2020 AM

Guardrail Loading Conditions

Unitorm Load

Per 2018 IBC §1607.8.1, the uniform load shall be applied to the handrail in any direction. This loading is only applicable to commercial projects with public access and is not applicable to residential guardrails. The railing system covered in this package covers all commercial and residential, thus this loading condition shall apply.

Concentrated Load

Per IBC §1607.8.1.1, the concentrated load shall be applied to

the handrail in any direction

Per IBC §1607.8.1.2, components including intermediate rails, balusters, and cables shall be designed for a concentrated load

applied normal and horizontally over an area of 1ft².

Per IBC §1015.4 and IRC §312.1.3 opening limitations shall not allow

the passage of a sphere 4" in diameter through.

p = 50 plf

P = 200 lbs

P = 50 lbs

	Part N	lumbers	and	Descri	ptions
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IP100 - SCS Extruded Aluminum Intermediate Posts Page 4, 5, 6 TR100 - SCS Extruded Aluminum Top Rail Page 7,8,9,10 FI200 - SCS Extruded Aluminum Flat Infill

EC100 - SCS Top Rail End Cap

BP100 - SCS Base Plate Page 11, 12 SR200 - SCS Extruded Aluminum Stair Rail Page 13

RCB100 - SCS Stair Grab Rail Connecting Block

Stainless Steel Wire Rope Page 14 TP100 - SCS Extruded Aluminum Termination Posts Page 15, 16 Page 17, 18

ISPA200 - SCS Stair Post Cap Assembly Intermediate Stair Post Adapter

Aluminum Cable Guardrail System Summary

1 or 2 Family Residential? Yes Total Post/Handrail Height Including Base Plate 42 in Maximum Post Spacing 5'-0" oc Maximum Stair Rail Post Spacing 5'-0" oc Cable Prestressing 255 lbs Cable Spacing (On-Center) 3.125 in



SUBJECT: Aluminum Calcs

DATE: **DESIGN:**

10/20/2020 AM

PAGE:

Extruded Aluminum Post Input

Post Spacing, s = 5 ft (See Page 3) Applied Load At Top, P = 200 lbs Unbraced Length = 40.5/8", LB = 40.63 in

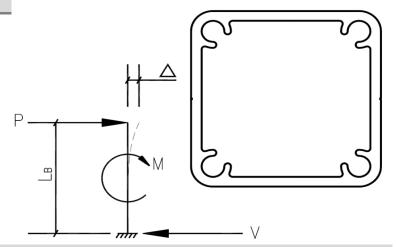
> 1.146 in² 10100 ksi Modulus of Elasticity, E = Section Modulus, S = 0.744 in³

Plastic Section Modulus, Z = 0.848 in³ Moment of Inertia, Imin = 0.837 in4 Torsion Constant, J = 0.073 in

Post Area, Ap =

Clear Height of Shear Area, h = 2.250 in Thickness of Shear Area, t = 0.125 in

> $C_b =$ 1.3 $k_t =$ 1.0



element supported on both edges, Table B.5.1

Flexural Yielding and Rupture 6061-T6 (ADM 2015 Section F.2)

Applied Moment, P*LB = Mapplied =

yielding moment strength, Mnp = 29.67 kip-in rupture moment strength, Mnu = 32.21 kip-in all other limit states, Ω_h = 1.65 rupture limit state, Ω_b = 1.95 Allowable Moment, M_{nmb}/Ω_b = 16.52 kip-in

Flexural Local Buckling 6061-T6 (ADM 2015 Section F.3, B.5.5.5, Table 2-19 Part VI)

Slenderness, $\lambda =$ 16.0 Slenderness, λ eq = 25.6

Fe = 152.0 ksi

8.13 kip-in

Controls

Allowable Stress, \lambda eq≤\lambda1 = 24.2 ksi

Slenderness Limit, $\lambda 1 =$ 33.5 Allowable Stress, $\lambda_1 < \lambda_2 = \lambda_2 = \lambda_1$

-169.4 ksi Slenderness Limit, $\lambda_2 =$ 61.0 Allowable Stress, λeq≥λ2 = 32.6 ksi Allowable Bending Stress, $Fb/\Omega =$

24.2 ksi Allowable Moment, $S*Fb/\Omega = Mallow =$ 17.98 kip-in

Applied Moment, P*LB = Mapplied = 8.13 kip-in

Flexural Lateral Torsional Buckling 6061-T6 (ADM 2015 Section F.4)

Slenderness, $\lambda =$ 22.3 for closed shape member, F.4.2.3 Controls

inelastic buckling, M_{nmb} = 19.86 ksi elastic buckling, M_{nmb} = 148.92 ksi

1.65

Allowable Moment, M_{nmb}/Ω_b = 12.03 kip-in Applied Moment, P*LB = Mapplied = 8.13 kip-in

Deflection Check, ΔMAX = LB/12 (ICC Report AC273)

Allowable Deflection, Δ allow = 3.385 in Applied Deflection, PLB³/3EI = Δ applied = 0.529 in OK

Shear in Elements, Gross Section 6061-T6 (ADM 2015 Table Section G.2, Table 2-19 Part VI)

Allowable Stress, λ≤λ1 = 12.7 ksi Slenderness Limit, λ1 = 35.3 Allowable Stress, $\lambda_1 < \lambda < \lambda_2 =$ 14.8 ksi Slenderness Limit, λ_2 = 63.0 Allowable Stress, λ≥λ2 = 151.0 ksi Allowable Shear Stress, F_s/Ω = 13 ksi

Allowable Shear, $Ap^*F_s/\Omega = Vallow =$ 14.557 kips Applied Shear, P = Vapplied = 0.200 kips



SUBJECT: Aluminum Calcs

DATE:

DESIGN:
PAGE:

10/20/2020 AM

Core Mounted Posts Bearing Check

Existing Concrete Strength, t'c = 2500 psi

Vapplied = 0.200 kips (See Page 4)
Mapplied from post = 8.125 kip-in (See Page 4)

Mapplied from shear = 0.600 kip-in

Mtotal = 8.725 kip-in

Depth of Concrete Blockout, dblockout = 3.000 in

Dist Bottom of Blockout to Applied Pu, dcompb = 2.000 in

Dist from Applied Pu to Top of Concrete, dcompt = 1.000 in

Width of Post, dterm = 2.250 in

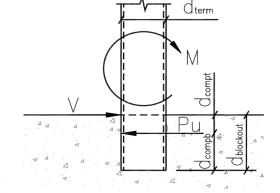
Loaded Area, $A1 = 2.250 \text{ in}^2$

Area of the Lower Base of Largest Fulcrum, $A2 = 6.500 \text{ in}^2$

Compression Load at Blockout, Pu = 4.363 kips

Strength Reduction Factor, $\emptyset = 0.65$ (Per ACI 318-14 §21.2) Concrete Bearing Strength, tb = 5282 psi (Per ACI 318-14 §22.8)

Maximum Applied Compression Load, fbmax = 1939 psi OK < 5282 psi



Core Mounted Posts Edge Distance Check

tance from Center of Post to Edge of Concrete, cal = 6.750 in

Distance from Post Face to Edge of Concrete, cpost = 4.500 in

Thickness of Concrete, hal = 4.000 in

Projected Concrete Failure Area, Avco = 205.031 in² (Per ACI 318-14 § 17.5.2.1) Projected Concrete Failure Area, Avc = 90.000 in² (Per ACI 318-14 § 17.5.2.1) Shear Strength Modification Factor, ψed, V = 1.00 (Per ACI 318-14 §17.5.2.6) Cracked Concrete Modification Factor, ψc, v = 1.00 (Per ACI 318-14 § 17.5.2.7) Cracked Concrete Modification Factor, wh, v = 1.59 (Per ACI 318-14 §17.5.2.8) Lightweight Concrete Factor, $\lambda =$ 1.00 (Per ACI 318-14 § 19.2.4.2)

Basic Concrete Breakout Strength, Vb = 9.752 kips (Per ACI 318-14 § 17.5.2.2)

Nominal Concrete Breakout Strength, Vcb = 6.811 kips (Per ACI 318-14 § 17.5.2.1)

Max Nominal Concrete Breakout Strength, Vmax = 6.811 kips OK < 4.3625 kips

Use 4,000psi Non-Shrink Grout in Min 3"SQx4"Deep Blockout or 3" Diax4"Deep Hole with 4 ½" Min Edge Distance (No Rebar) or 1 ¼" Min Edge Distance when #3 or Larger Slab Edge Rebar Present

Check Top Connection

Note: Lateral loads on top rail bears directly on post side. Only uplift loads affecting attachment are considered.

Diameter of Screw, dscrew = 0.194 in

Thickness of Post, tpost = 0.125 in

Area of Engaged Post in Shear, Avpost = 0.024 in^2

Number of Screws in Shear = 2

Factor of Safety on Screw Connections, $n_s = 3.00$

Tensile Ultimate Strength of Member Not

in Contact with Screw Head, Ftu2 = 38 ksi

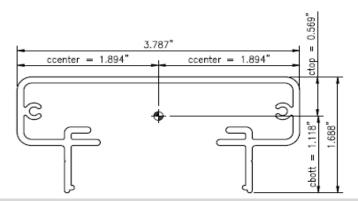
Shear Strength of Screw, Vscrew = 0.614 kips OK > 0.250 kips



SUBJECT: Aluminum Calcs

DATE: __ DESIGN: $\frac{10/20/2020}{AM}$

PAGE:



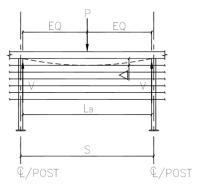
Extruded Aluminum Rail Input

Post Spacing, s = 5 ft (See Page 4) Applied Load At Top, P = 200 lbs Unbraced Length, $LB = 5'-0" \times 12" - 2.25" =$ 57.750 in Compressive Modulus of Elasticity, E = 10100 ksi Rail Area, Ar = 0.928 in² Moment of Inertia x, Ixx = 0.212 in4 Moment of Inertia y, lyy = 1.664 in⁴ Top of Member to Centroid, ctop = 0.569 in

> C_{b} = 1.118 in C_{b} = 1.31 k_{t} = 1.0

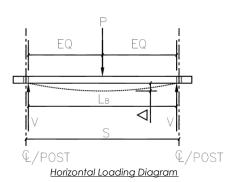
Lett/Right to Centroid, Ccenter = 1.895 in Section Modulus Top, Sxx = 0.373 in³ Section Modulus Bottom, Sxx = 0.190 in³ Section Modulus Top, Zxx = 0.560 in³ Section Modulus Bottom, Zxx = 0.285 in³ Section Modulus, Syy = 0.879 in³ Torsion Constant, J = 0.005 in Clear Height of Shear Area, h = 1.643 in

0.090 in



Bottom of Member to Centroid, cbott =

Vertical Loading Diagram



Thickness of Shear Area, t =

Flexural Yielding and Rupture 6061-T6 (ADM 2015 Section F.2)

yielding moment strength, Mnp = 9.97 kip-in rupture moment strength, Mnu = 10.83 kip-in all other limit states, $\Omega_{\rm b}$ = 1.65 rupture limit state, $\Omega_{\rm b}$ = 1.95 Allowable Moment, $M_{\rm nmb}/\Omega_{\rm b}$ = 5.55 kip-in Applied Moment, P*s/4 = Mapplied = 0.25 kip-in OK



■ Controls

Controls

SUBJECT: Aluminum Calcs

DATE: DESIGN: PAGE:

element supported on both edges, Table B.5.1

10/20/2020 AM

Flexural Local Buckling 6061-T6 (ADM 2015 Section F.3, B.5.5.5, Table 2-19 Part VI)

10.69

Slenderness, λeq = 17.1

Fe = 341 ksi

Allowable Stress, λ≤λ1 = 31.8 ksi Slenderness Limit, λ1 = 33.5

Allowable Stress, $\lambda_1 < \lambda < \lambda_2 =$ -215.9 ksi

Slenderness Limit, $\lambda_2 =$ 61.0 Allowable Stress, λ≥λ2 = 48.8 ksi

Allowable Bending Stress, Fb/Ω = 31.8 ksi Allowable Moment, $S*Fb/\Omega = Mallow =$ 6.04 kip-in

Applied Moment, P*s/4 = Mapplied =0.25 kip-in

Flexural Lateral Torsional Buckling 6061-T6 (ADM 2015 Section F.4)

> $d_{top}=$ 3.787 in

 $t_{top} =$ 0.090 in

Area of top element = 0.340 in³

> $d_{side} =$ 1.138 in

0.090 in $t_{\text{side}} =$ 0.102 in³

Area of side element = Slenderness, $\lambda =$ 32.3 any shape F4.2.5

18.12 kip-in Me =

U =0.49 go= 0.000 in

C1 =0.50 C2 =

0.50 -1.94 Bx =

Shear Center, yo = 1.12

inelastic buckling, M_{nmb} = 5.19 ksi elastic buckling, M_{nmb} = 32.46 ksi

1.65

Allowable Moment, M_{nmb}/Ω_b = 3.14 kip-in Applied Moment, P*s/4 = Mapplied =0.25 kip-in OK

Deflection Check, ΔMAX = LB/12 (ICC Report AC273)

Allowable Detlection, Δ ALLOW = 4.813 in

Applied Deflection, PLB³/48EI = Δ APPLIED = 0.374 in OK

Shear in Elements, Gross Section 6061-T6 (ADM 2015 Table Section G.2, Table 2-19 Part VI)

Slenderness, $\lambda =$ 10.69 Allowable Stress, λ≤λ1 =

12.7 ksi ■ Controls Slenderness Limit, λ1 = 35.3 in³

Allowable Stress, $\lambda_1 < \lambda < \lambda_2 =$ 15.357 ksi

> Slenderness Limit, λ2 = 63 in³

Allowable Stress, λ≥λ2 = 338.650 ksi Allowable Shear Stress, $F_s/\Omega =$

12.7 ksi Allowable Shear, $Ap^*F_s/\Omega = V_{allow} =$ 11.780 kips

> Applied Shear, $P = V_{applied} =$ 0.200 kips **OK**



SUBJECT: Aluminum Calcs

DATE: __ DESIGN: 10/20/2020 AM

¥/SCREW

PAGE:

Tension Capacity of Screw (ADM 2015 Section J5.4, AISC DG 27)

 $M_{APPLIED} = 8.125 \text{ kip-in}$

(Page 4)

Number of Screws in Tension = 2

Resisting Moment Arm, Center of Screw to Compression Face, larm = 2.000 in

Tension Applied, Papplied = 2.0313 kips

Thread Stripping Area of Internal Thread Per Inch, $A_{sn} = 0.663 \text{ in}^2$

Depth of Full Thread Engagement into tube, Le = 1.000 in

Tensile Ult Strength of Member Not in Contact with Screw Head, Ftu2 = 38 ksi

Nominal Pull-Out Strength, Rn = 14.613 kips

(Eq. J.5-3)

Thickness of Member in Contact with Screw Head, t₁ = 0.375 in

Tensile Yield Strength of Member in Contact with Screw Head, Fty₁ = 35 ksi

Member in Confact with Screw Head, Fty1 = 35 ksiNominal Screw Head Diameter Abs Min, D = 0.568 in

os Min, D = 0.568 in $t_1/D = 0.66$

Nominal Pull-Over Strength, Rn = 9.150 kips

(Eq. J5-10)

<1.1

Tensile Strength of Screw, Fnt = 56 ksi Stainless Steel

Tensile Stress Area of Screw, $A_s = 0.077 \text{ in}^2$

Nominal Tensile Strength of a Screw, Rn = 4.312 kips (Eq. AISC DG 27 Eq. J3-1)

 Ω , Aluminum = 3.00

 Ω , Steel = 2.00

Pull-Out Strength, Rn/ Ω = 4.871 kips OK > 2.03125 kips Pull-Over Strength, Rn/ Ω = 3.050 kips OK > 2.03125 kips Tensile Strength, Rn/ Ω = 2.156 kips OK > 2.03125 kips

Shear Capacity of Screw (ADM 2015 J5.5, AISC DG 27)

 $V_{APPLIED} = 3.515 \text{ kips}$

Number of Screws in Shear = 4

Shear Applied, Vapplied = 0.879 kips Per Screw

diameter of screw, d = 0.313 in

Tensile Ultimate Strength of Member in Contact with Screw Head, Ftu = 38 ksi Note: 1/2 of depth subtracted from to

dist from screw center to edge of connected part, de = 0.500 in as screw is countersunk

thickness of connected part, t = 0.375 in

Screw Bearing Strength, Rn = 3.563 kips (Eq. J.5-12)

Shear Strength of Screw, Fnv = 34 ksi Stainless Steel

Shear Stress Area of Screw, $A_s = 0.077 \text{ in}^2$

Nominal Shear Strength of a Screw, Rn = 2.587 kips (Eq. AISC DG 27 Eq. J3-1)

 Ω , Aluminum = 3.00

 Ω , Steel = 2.00

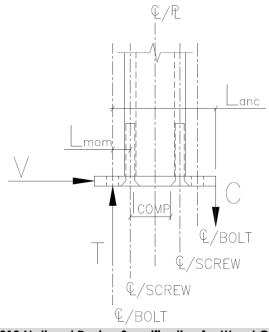
Bearing Strength, $Rn/\Omega = 1.188$ kips OK > 0.87875 kips Shear Strength, $Rn/\Omega = 1.294$ kips OK > 0.87875 kips



SUBJECT: Aluminum Calcs

DATE: DESIGN: 10/20/2020

PAGE:



Base Plate Anchorage (Lag Screws) Per 2018 National Design Specification for Wood Construction

Applied Moment at IP100, Mapplied = 8.125 kip-in (Page 4)

Edge of Baseplate to Centerline of Tension Anchorage, lanc = 4.360 in

> Number of Screws in Tension = 2

Applied Tension at Anchor Bolt/Screw, Tapplied = 0.932 kips

> Vapplied = 0.200 kips (Page 4)

Number of Screws in Shear =

Shear Applied, Vapplied = 0.050 kips **Per Screw**

Lag Screw Ref Withdrawl Design Value (G=0.46, D=3/8"), W = 214 lbs (Per Simpson Strong-Tie)

> Penetration Depth, d = 4.500 in

Allowable Lag Screw Tension, Tallowable =

1.541 kips OK > 0.932 kips

Lag Screw Reference Lateral Design Value (G=0.46, D=3/8"), Z = 405 lbs (Per Simpson Strong-Tie)

Allowable Lag Screw Shear, Vallowable = 0.405 kips OK > 0.05 kips

> Use (4) Simpson 0.220" Dia x 6" SDWS Timber Screw with 6" Min Penetration into Min (1) 6x6 or (2) 3x6 Hem-Fir #2 (1.5" Min Edge Distance)

Base Plate Anchorage (Thru-Bolts) Per 2018 National Design Specification for Wood Construction

Bolt diameter = 0.375 in

Diameter of washer = 2.500 in

Area of Bearing under washer = 4.758 in²

Washer bearing, $F_{c perp} =$ 521 psi (Per Table 4A)

Allowable Thru-Bolt Tension, Tallowable = 2.209 kips OK > 0.932 kips

Lag Screw Reference Lateral Design Value (G=0.46, D=3/8"), Z = 405 lbs (No Thru-Bolt Values < 1/2" In NDS - Use Table 11K)

> Allowable Thru-Bolt Shear, Vallowable = 0.405 kips OK > 0.05 kips

> > Use (4) %" Dia SS304 Thru-Bolts with Min 2" Dia Heavy Washer into Min (1) 6x or (2) 3x Hem-Fir #2

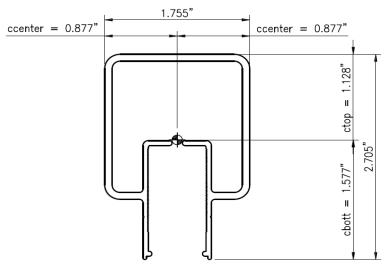


SUBJECT: Aluminum Calcs

DATE: **DESIGN:**

10/20/2020 AM

PAGE:



Extruded Aluminum Stair Rail Input

Post Spacing, s = 5 ft 200 lbs

Applied Load At Top, P = Unbraced Length, LB = 6'x12''-2.25'' =57.750 in Compressive Modulus of Elasticity, E = 10100 ksi

Rail Area, Ar = 0.761 in²

Moment of Inertia x, Ixx = 0.467 in4

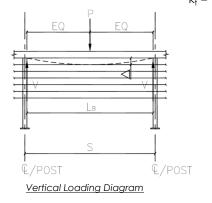
Moment of Inertia y, lyy = 0.307 in⁴

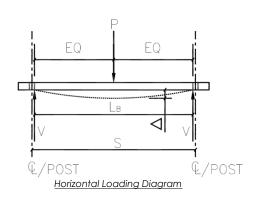
Top of Member to Centroid, ctop = 1.128 in Bottom of Member to Centroid, cbott = 1.577 in

> C_b = 1.0 $k_t =$ 1.0

> > 1.95

Lett/Right to Centroid, Ccenter = 0.878 in Section Modulus Top, Sxx = 0.414 in³ Section Modulus Bottom, Sxx = 0.296 in³ Section Modulus Top, Zxx = 0.621 in³ Section Modulus Bottom, Zxx = 0.444 in³ Section Modulus, Syy = 0.350 in³ Torsion Constant, J = 0.005 in Clear Height of Shear Area, h = 2.660 in Thickness of Shear Area, t = 0.090 in





Flexural Yielding and Rupture 6061-T6 (ADM 2015 Section F.2)

yielding moment strength, Mnp = 15.55 kip-in rupture moment strength, Mnu = 16.88 kip-in all other limit states, Ω_b = 1.65

rupture limit state, Ω_b = Allowable Moment, M_{nmb}/Ω_b = 8.66 kip-in

Applied Moment, P*s/4 = Mapplied = 0.25 kip-in OK



SUBJECT: Aluminum Calcs

■ Controls

Controls

element supported on both edges, Table B.5.1

DATE: DESIGN: PAGE: 10/20/2020 AM

Flexural Local Buckling 6061-T6 (ADM 2015 Section F.3, B.5.5.5, Table 2-19 Part VI)

Slenderness, $\lambda = 19.53$

Slenderness, $\lambda eq = 31.3$

Fe = 102 ksi

Allowable Stress, λ≤λ1 = 31.8 ksi

Slenderness Limit, $\lambda 1 = 33.5$ Allowable Stress, $\lambda 1 < \lambda < \lambda 2 = -436.7$ kg

Slenderness Limit, $\lambda 2 = -436.7$ ksi Slenderness Limit, $\lambda 2 = 61.0$ Allowable Stress, $\lambda \ge \lambda 2 = 26.7$ ksi

Allowable Stress, $\lambda \ge \lambda 2 = 26.7$ ksi Allowable Bending Stress, Fb/ $\Omega = 31.8$ ksi Allowable Moment, S*Fb/ $\Omega = Mallow = 9.42$ kip-

Allowable Moment, $S*Fb/\Omega = Mallow = 9.42$ kip-in

Applied Moment, P*s/4 = Mapplied = 0.25 kip-in

OK

Flexural Lateral Torsional Buckling 6061-T6 (ADM 2015 Section F.4)

 $d_{top} = 3.787 \text{ in}$

 $t_{top} = 0.090 in$

Area of top element = 0.340 in³

 $d_{side} = 1.138 in$

 $t_{\text{side}} = 0.090 \text{ in}$

Area of side element = 0.102 in^3 Slenderness, $\lambda = 35.3$ a

ness, $\lambda = 35.3$ any shape F4.2.5

Me = 23.66 kip-in U = 0.53

go = 0.000 in

C1 = 0.50C2 = 0.50

Bx = -2.11

Shear Center, yo = 1.58

inelastic buckling, $M_{nmb} = 7.31 \text{ ksi}$

elastic buckling, $M_{nmb} = 27.18 \text{ ksi}$

 $_{b} = 1.65$

Allowable Moment, $M_{nmb}/\Omega_b = 4.43$ kip-in Applied Moment, P*s/4 = Mapplied = 0.25 kip-in OK

Deflection Check, ΔMAX = LB/12 (ICC Report AC273)

Allowable Deflection, Δ ALLOW = 4.813 in

Applied Deflection, PLB³/48EI = Δ APPLIED = 0.170 in **OK**

Shear in Elements, Gross Section 6061-T6 (ADM 2015 Table Section G.2, Table 2-19 Part VI)

Slenderness, $\lambda = 19.53$

Allowable Stress, $\lambda \leq \lambda 1 = 12.7 \text{ ksi}$ < Controls

Slenderness Limit, $\lambda 1 = 35.3 \text{ in}^3$

Allowable Stress, $\lambda 1 < \lambda < \lambda 2 = 14.410 \text{ ksi}$

Slenderness Limit, $\lambda 2 = 63 \text{ in}^3$

Allowable Stress, $\lambda \ge \lambda 2 = 101.330 \text{ ksi}$ Allowable Shear Stress, $F_5/\Omega = 12.7 \text{ ksi}$

Allowable Shear, $Ap^*F_s/\Omega = V_{allow} = 9.665 \text{ kips}$

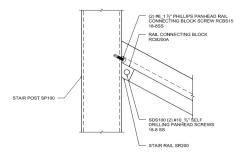
Applied Shear, P = Vapplied = 0.200 kips OK



SUBJECT: Aluminum Calcs

DATE: 10/20/2020 DESIGN: AM

PAGE:



Tension Capacity of Screw (ADM 2015 Section J5.4, AISC DG 27) SDS100

Note: Uses (2) #10_3/4" Phillips Pan Head Sheet Metal Screws - Type A, 18-8 Stainless Steel

Tension Load = 0.200 kips (Page 4)

Screw Diamter, d = 0.138 in

Number of Screws = 2

Screw Tension Load = 0.100 kips (Page 4)

Thread Stripping Area of Internal Thread Per Inch, $Asn = 0.401 \text{ in}^2$ (Table 5-6)

Depth of Full Thread Engagement into tube, Le = 0.500 in Tensile Ult Strength of Member Not in Contact with Screw Head, Ftu2 = 38 ksi

Nominal Pull-Out Strength, Rn = 4.419 kips (Eq. J.5-3)

Thickness of Member in Contact with Screw Head, h = 0.050 in Tensile Yield Strength of Member in Contact with Screw Head, h = 0.050 in 35 ksi

Nominal Screw Head Diameter Abs Min, D = 0.376 in

 $t_1/D = 0.13 < 1.1$

Nominal Pull-Over Strength, Rn = 0.305 kips

(Eq. J5-10)

Tensile Strength of Screw, Fnt = 49 ksi 18-8 Stainless Steel

Tensile Stress Area of Screw, $A_s = 0.015 \text{ in}^2$

isile Strength of a Screw, Rn = 0.729 kips (Eq. AISC DG 27 Eq. J3-1)

Ω, Aluminum = 3.00 Ω, Steel = 2.00

Pull-Out Strength, $Rn/\Omega = 1.473$ kips OK > 0.1 kips Pull-Over Strength, $Rn/\Omega = 0.102$ kips OK > 0.1 kips Tensile Strength, $Rn/\Omega = 0.364$ kips OK > 0.1 kips

Screw Capacity of Screw (ADM 2015 Section J5.5, AISC DG 27) RCB515

Note: Uses (1) #6 x 1 1/2 Phillips Pan Head Screws - Type A, 18-8 Stainless Steel

Shear Load = 0.200 kips (Page 4)

Number of Screws in Shear =

Screw Shear Load = 0.200 kips

Tensile Ultimate Strength of Member in Contact with Screw Head, Ftu = 38 ksi

dist from screw center to edge of connected part, de = 0.500 in

thickness of connected part, t = 0.125 in

Screw Bearing Strength, Rn = 1.311 kips (Eq. J.5-12)

Shear Strength of Screw, Fnv = 29 ksi 18-8 Stainless Steel

Screw Diamter, d = 0.138 in

Shear Stress Area of Screw, $A_s = 0.015 \text{ in}^2$

Nominal Shear Strength of a Screw, Rn = 0.437 kips (Eq. AISC DG 27 Eq. J3-1)

 Ω , Aluminum = 3.00

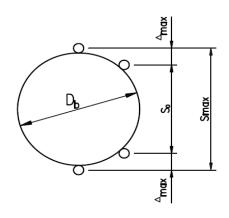
 Ω , Steel = 2.00

Bearing Strength, $Rn/\Omega = 0.437$ kips OK > 0.2 kips Shear Strength, $Rn/\Omega = 0.219$ kips OK > 0.2 kips

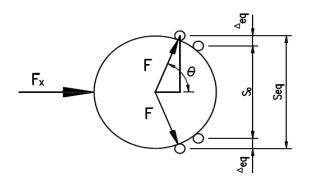


SUBJECT: Aluminum Calcs

DATE: DESIGN: PAGE: 10/20/2020 AM



Initial and Pass—Through Conditions



Conditions at Equilibrium

Check Cable Deflection

Note: A min load of 50psf shall be applied to a 4" sphere. Spacing and deflection of the cables shall not allow the sphere to pass through.

Diameter of Cable, D = 0.125 in Intermediate Post Spacing, L = 5 ft Prestress Force, Fps = 255 ft Sphere Diameter, Db = 4.000 in Initial Cable Spacing, So = 3.125 in Termination Post Spacing, LT = 30 ft Load Applied to Sphere, wsphere = 50.0 psf Projected Area of Sphere, Asphere = 12.566 in² Impact Factor, If = 2.00 Force Applied to Sphere, Fxsphere = 8.727 lbs Spread at Pass-Thru = Db+Dcable, Smax = 4.125 in Final Cable Spacing, Sfinal = Seq = 4.124 in Deflection at Pass-Thru = (Smax-So)/2, $\Delta'max =$ 0.500 in Deflection, $\Delta = \Delta_{eq} =$ 0.500 Applied Angle = $asin((S_0+2\Delta)/(D_b+D))$, θ = 88.7° Force Applied to Cable, T = F = 198.171 lbs Maximum Cable Deflection = (Db+D-So)/2, $\Delta max =$ 0.500 in Modulous of Elasticity, E = 29000 ksi $P_{ef} = \frac{4\Delta EA}{L} \times \frac{\sqrt{4\Delta^2 + L^2} - L}{\sqrt{4\Delta^2 + L^2} + L_T - L}$ Moment of Inertia, I = 0.00001198 in4 Cross Sectional Area, A = 0.012 in² Extensible, Flexible Cable, Pef = 0.274 lbs Flexural Bending, Pb = 0.039 lbs Prestressing, Pps = 8.492 lbs Force in Cable Resisting Sphere, Fxcable = P = 8.804 lbs 1/8" Diameter 1x19 Strand Core Breaking Strength = 1869 lbs 1/8" Diameter 7x7 Strand Core Breaking Strength = 1566 lbs ◆ Controls (OK < 310lbs)
</p>



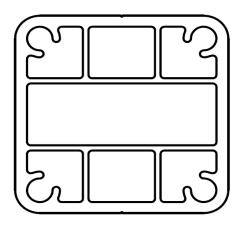
SUBJECT: Aluminum Calcs

DATE: **DESIGN:** PAGE:

10/20/2020 AM

Extruded Aluminum Termination Post Input

Post Spacing, s = 5'-0" oc Prestress Force, Fps = 255 lbs (Page 11) Initial Cable Spacing, So = 3.125 in Unbraced Length = 40 5/8", LB = 40.63 in Distributed Load, w = 81.6 lb/in Post Area, Ap = 1.529 in² Modulus of Elasticity, E = 10100 ksi Section Modulus, S = 0.847 in³ Approx. Plastic Section Modulus, Z = 1.032 in³ Moment of Inertia, I = 0.953 in4 Approx. Torsion Constant, J = 0.143 in Clear Height of Shear Area, h = 2.250 in Thickness of Shear Area, t = 0.125 in 2.1 $k_{t} =$ 1.0 Shear Load from Point Load, V_{applied} = 200 lbs (Page 4) Shear Load from Cable Prestress, V_{applied} = 3315 lbs Shear from Point Load and Cable, V_{tot} = 3515 lbs



*At end post, applied moments do not occur at same location along length of cross section (i.e. base vs mid point), therefore max moment will govern design. At corner post, field test for bi-directional bending due to 90° cable turn.

Flexural Yielding and Rupture 6061-T6 (ADM 2015 Section F.2)

Moment From Point Load, Mpnt *=

Moment From Cable Prestress, Mpstr *=

Tensile Rupture Capacity, Ftu = 38.0 ksi Tensile Yield Capacity, Fty = 35.0 ksi Compression Yield Capacity, Fcy = 35.0 ksi yielding moment strength, Mnp = 36.13 kip-in rupture moment strength, Mnu = 39.23 kip-in all other limit states, Ω_b = 1.65 rupture limit state, Ω_b = 1.95 Allowable Moment, M_{nmb}/Ω_b = 20.12 kip-in

Applied Moment, M = 16.834 kip-in DCR = 0.84

8.125 kip-in

16.834 kip-in

■ Controls

Flexural Local Buckling 6061-T6 (ADM 2015 Section F.3, B.5.5.5, Table 2-19 Part VI)

Slenderness, $\lambda =$ 6.10 9.8 Slenderness, λeq = 1046.8 ksi Fe = Allowable Stress, λeq≤λ1 = 23.0 ksi

element supported on both edges, Table B.5.1

Controls

Slenderness Limit, λ1 = 33.3 Allowable Stress, $\lambda_1 < \lambda_{eq} < \lambda_2 =$ -56.5 ksi Slenderness Limit, λ2 = 61.0 Allowable Stress, λeq≥λ2 = 85.5 ksi Allowable Bending Stress, Fb/Ω = 23.0 ksi

Allowable Moment, $S*Fb/\Omega = Mallow =$ 19.46 kip-in

> Applied Moment, M = 16.834 kip-in OK DCR = 0.86



SUBJECT: Aluminum Calcs

DATE: DESIGN:

PAGE:

10/20/2020 AM

Flexural Lateral Torsional Buckling 6061-T6 (ADM 2015 Section F.4)

Slenderness, $\lambda = 15.4$ for closed shape member, F.4.2.3

inelastic buckling, M_{nmb} = 27.98 ksi **◄** Controls

elastic buckling, $M_{nmb} = 357.39 \text{ ksi}$

 $\Omega_{\rm b} = 1.65$

Allowable Moment, $M_{nmb}/\Omega_b = 16.96$ kip-in

Applied Moment, M = 16.834 kip-in OK DCR = 0.99

Deflection Check, Δ MAX = LB/12 (ICC Report AC273)

Allowable Deflection, Δ allow = 3.385 in

Applied Deflection, $PLB^3/3EI = \Delta applied = 0.592 in$

Shear in Elements, Gross Section 6061-T6 (ADM 2015 Table Section G.2, Table 2-19 Part VI)

Allowable Stress, $\lambda \le \lambda 1 = 12.7 \text{ ksi}$ < Controls

Slenderness Limit, $\lambda 1 = 35.3$ Allowable Stress, $\lambda 1 < \lambda < \lambda 2 = 15.8$ ksi

Slenderness Limit, $\lambda 2 = 63.0$ Allowable Stress, $\lambda \ge \lambda 2 = 1040.5$ ksi Allowable Shear Stress, Fs/ $\Omega = 13$ ksi

Allowable Shear, $Ap*F_s/\Omega = V_{allow} = 19.418 \text{ kips}$

Applied Shear, Vtot = 3.515 kips OK



SUBJECT: Aluminum Calcs

DATE: _ DESIGN: $\frac{10/20/2020}{\Delta M}$

PAGE:

Extruded Aluminum Stair Handrail Connection Input

Post Spacing, s = 5 ft Force, F = 200 lbs (Page 4) Moment Arm = 2.750 in Initial Cable Spacing, So = 0.000 in Unbraced Length, LB = 1.600 in Post Area, Ap = 0.531 in² Compressive Modulus of Elasticity, E = 10100 ksi Compression Section Modulus, Sy = 0.079 in³ Compression Section Modulus, Zy = 0.118 in³ Moment of Inertia, ly = 0.019 in4

C_b =

 $k_t =$

J = 0.096 in⁴
Sx = 0.178 in³
Sy = 0.079 in³
Ix = 0.100 in⁴
Iy = 0.019 in⁴
Area = 0.531 in²
wall/thick = 13.000

■ Controls

Controls

OK

11 =

t2 =

a =

b =

0.125 in

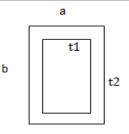
0.125 in

0.625 in

1.750 in

element supported on both edges, Table B.5.1

for closed shape member, F.4.2.3



Flexural Yielding and Rupture 6061-T6 (ADM 2015 Section F.2)

Torsion Constant, J =

Moment From Railing, M =

yielding moment strength, Mnp = 4.14 kip-in rupture moment strength, Mnu = 4.49 kip-in all other limit states, $\Omega_{\rm b}$ = 1.65 rupture limit state, $\Omega_{\rm b}$ = 1.95 Allowable Moment, $M_{\rm nmb}/\Omega_{\rm b}$ = 2.30 kip-in Applied Moment, Mapplied = 0.55 kip-in OK

0.096 in4

0.550 kip-in

1.3

1.0

Flexural Local Buckling 6061-T6 (ADM 2015 Section F.3, B.5.5.5, Table 2-19W Part VI)

Slenderness, $\lambda = 12.00$ Slenderness, $\lambda eq = 19.2$

Fe = 270.1 ksi

Allowable Stress, λ≤λ1 = 31.8 ksi

Slenderness Limit, $\lambda 1 = 45.1$

Allowable Stress, $\lambda 1 < \lambda < \lambda 2 =$ -486.4 ksi Slenderness Limit, $\lambda 2 =$ 123.0

Allowable Stress, $\lambda \ge \lambda 2 = 28.9 \text{ ksi}$ Allowable Bending Stress, Fb/ $\Omega = 31.8 \text{ ksi}$

Allowable Moment, $S*Fb/\Omega = Mallow = 2.51$ kip-in Applied Moment, Mapplied = 0.55 kip-in OK

Flexural Lateral Torsional Buckling 6061-T6 (ADM 2015 Section F.4)

Slenderness, $\lambda = 3.5$ inelastic buckling, $M_{nmb} = 3.94$ ksi elastic buckling, $M_{nmb} = 646.25$ ksi

 $\Omega_{\rm b} = 1.65$

Allowable Moment, $M_{nmb}/\Omega_b = 2.39$ kip-in Applied Moment, Mapplied = 0.55 kip-in OK

Deflection Check, ΔMAX = LB/12 (ICC Report AC273)

Allowable Deflection, Δ allow = 0.133 in Applied Deflection, PLB³/3EI = Δ applied = 0.001 in



SUBJECT: Aluminum Calcs

DATE: <u>10/20/2020</u> DESIGN: <u>AM</u>

PAGE:

Shear in Elements, Gross Section 6061-T6 (ADM 2015 Table Section G.2, Table 2-19W Part VI)

Allowable Stress, $\lambda \le \lambda 1 = 5.1$ Controls Slenderness Limit, $\lambda 1 = 47.5$ Allowable Stress, $\lambda 1 < \lambda < \lambda 2 = 7.1$ ksi Slenderness Limit, $\lambda 2 = 126.0$ Allowable Stress, $\lambda \ge \lambda 2 = 1486.5$ ksi

Allowable Shear Stress, $F_s/\Omega = 5 \text{ ksi}$ Allowable Shear, $Ap^*F_s/\Omega = Vallow = 2.709 \text{ kips}$

Allowable Streat, Ap Ps/32 - Vallow - 2.707 kipsApplied Shear, P = Vapplied = 0.200 kips OK

Weld Strength at Base (ADM 2015 J.2.5)

Nominal Strength of weld, $F_{nw} = 20 \text{ ksi}$ Table A3.3

Base Metal Strength, $F_{nBM} = 14 \text{ ksi}$ Table A3.6

Fillet Weld Size, Sw = 0.188 in

Effective Fillet Weld Size, Swe = 0.133 in

Weld Section Modulus, S = 0.086 in³

Base Metal Area, $Aw = 0.328 \text{ in}^2$

 $\Omega = 1.95$

Allowable Base Metal Strength, $F_{nBM}/\Omega = 7.385$ ksi

Applied Metal Stress, (M/a)/Aw = 2.682 ksi OK Allowable Weld Strength, $F_{nw}/\Omega = 10.043 \text{ ksi}$

Applied Weld Stress, M/S = 6.390 ksi

Shear Capacity of Screw at Top fo Handrail (ADM 2015 J5.6) #6 x 1 1/2"_RCBS200

 $V_{APPLIED} = 0.200 \text{ kips}$

Number of Screws in Shear = 1

Shear Applied, Vapplied = 0.200 kips Per Screw

diameter of screw, d = 0.138 in

ille Ultimate Strength of Member in Contact with Screw Head, Ftu = 38 ksi

dist from screw center to edge of connected part, de = 0.250 in

thickness of connected part, t = 0.140 in

Screw Bearing Strength, Rn = 1.330 kips (Eq. J.5-12)

Shear Strength of Screw, Fnv = 34 ksi Stainless Steel

Shear Stress Area of Screw, $A_s = 0.015 \text{ in}^2$

Nominal Shear Strength of a Screw, Rn = 0.505 kips (Eq. AISC DG 27 Eq. J3-1)

 Ω , Aluminum = 3.00

 Ω , Steel = 2.00

Bearing Strength, $Rn/\Omega = 0.443$ kips OK > 0.2 kips Shear Strength, $Rn/\Omega = 0.252$ kips OK > 0.2 kips



Company:	Waypoint Engineering	Date:	9/5/2018
Engineer:	JF	Page:	1/5
Project:	Stainless Cable Solutions Concrete	e Anchor	age
Address:	601 Main Street #400		
Phone:	360.635.6611		
E-mail:	jared@waypointwa.com		

1.Project information

Customer company: Stainless Cable Solutions

Customer contact name: Customer e-mail: Comment: Project description: Location: Portland, Oregon Fastening description:

2. Input Data & Anchor Parameters

General

Design method:ACI 318-14 Units: Imperial units

Anchor Information:

Anchor type: Concrete screw Material: Stainless Steel Diameter (inch): 0.375

Nominal Embedment depth (inch): 3.250 Effective Embedment depth, her (inch): 2.040

Code report: IAPMO UES ER-493

Anchor category: 1 Anchor ductility: Yes h_{min} (inch): 5.00 c_{ac} (inch): 5.50 C_{min} (inch): 1.75 S_{min} (inch): 3.00

Base Material

Concrete: Normal-weight

Concrete thickness, h (inch): 5.00

State: Uncracked

Compressive strength, f'c (psi): 3000

Ψ_{c,V}: 1.4

Reinforcement condition: B tension, B shear

Supplemental reinforcement: No Reinforcement provided at corners: No Ignore concrete breakout in tension: No Ignore concrete breakout in shear: No Ignore 6do requirement: Not applicable

Build-up grout pad: No

Base Plate

Length x Width x Thickness (inch): 5.00 x 5.00 x 0.35

Yield stress: 34084 psi

Profile type/size: HSS2-1/4X2-1/4X1/8

Recommended Anchor

Anchor Name: Titen HD® Stainless Steel - 3/8"Ø SS Titen HD, hnom:3.25" (83mm)

Code Report: IAPMO UES ER-493



SCS PART# CCA 100-4
TITEN CONCRETE ANCHR 4" x 3/8"_304 SS

Note: Periodic special inspection is required per section 4.4 of the noted code report.

ANCHORAGE INTO CONCRETE IN LIEU OF SDWS TIMBER SCREWS



Company:	Waypoint Engineering	Date:	9/5/2018			
Engineer:	JF	Page:	2/5			
Project:	Stainless Cable Solutions Concret	Stainless Cable Solutions Concrete Anchorage				
Address:	601 Main Street #400					
Phone:	360.635.6611					
E-mail:	jared@waypointwa.com					

Load and Geometry

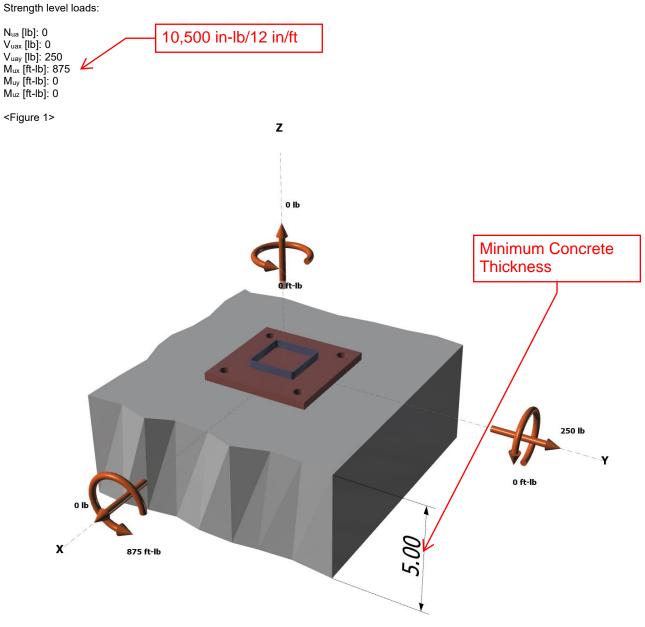
Load factor source: ACI 318 Section 5.3

Load combination: not set Seismic design: No

Anchors subjected to sustained tension: Not applicable

Apply entire shear load at front row: No

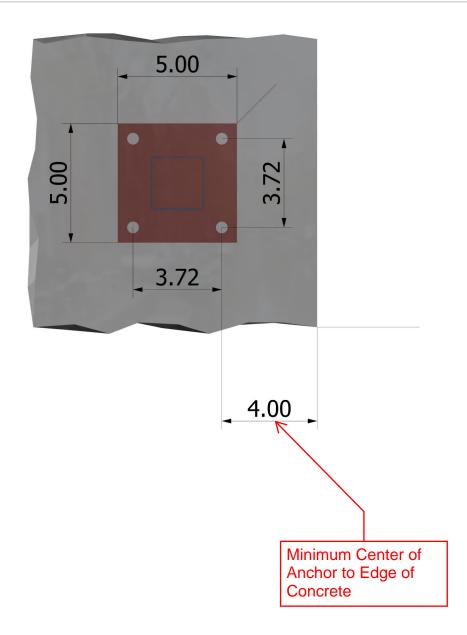
Anchors only resisting wind and/or seismic loads: No





Company:	Waypoint Engineering	Date:	9/5/2018			
Engineer:	JF	Page:	3/5			
Project:	Stainless Cable Solutions Concrete Anchorage					
Address:	601 Main Street #400					
Phone:	360.635.6611					
E-mail:	jared@waypointwa.com					

<Figure 2>





Company:	Waypoint Engineering	Date:	9/5/2018
Engineer:	JF	Page:	4/5
Project:	Stainless Cable Solutions Concret	e Anchor	age
Address:	601 Main Street #400		
Phone:	360.635.6611		
E-mail:	jared@waypointwa.com		

3. Resulting Anchor Forces

Anchor	Tension load, N _{ua} (lb)	Shear load x, V _{uax} (lb)	Shear load y, V _{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2+(V_{uay})^2}$ (lb)	
1	0.0	0.0	62.5	62.5	
2	1355.2	0.0	62.5	62.5	
3	1355.2	0.0	62.5	62.5	
4	0.0	0.0	62.5	62.5	
Sum	2710.3	0.0	250.0	250.0	

Maximum concrete compression strain (%): 0.17

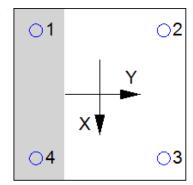
Maximum concrete compression stress (psi): 742

Resultant tension force (lb): 2710

Resultant compression force (lb): 2711

Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00 Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00 Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00 Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

Nsa (lb)	ϕ	ϕN_{sa} (lb)
12177	0.75	9133

5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

f'c (psi)

 $N_b = k_c \lambda_a \sqrt{f'_c h_{ef}}^{1.5}$ (Eq. 17.4.2.2a)

		. ,	. ,		` ,				
24.0	1.00	3000	2.040	383	30				
/A/ - / / A	/ A \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7()7()7(A	1 (0 17.0.1	0 = 4740	46)				
$\phi N_{cbg} = \phi (A$	$Nc/ANco)$ $\mathcal{P}ec,N$	$\mathscr{V}_{ed,N} \mathscr{V}_{c,N} \mathscr{V}_{cp,N} N$	b (Sec. 17.3.1	& Eq. 17.4.2	.10)				
A_{Nc} (in ²)	A_{Nco} (in ²)	c _{a,min} (in)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (Ib
60.22	37.45	4.00	1.000	1.000	1.00	0.727	3830	0.65	2911
00.22	37.43	4.00	1.000	1.000	1.00	0.727	3630	0.03	2911

N_b (lb)

hef (in)

8. Steel Strength of Anchor in Shear (Sec. 17.5.1)

V_{sa} (lb)	$\phi_{ extit{grout}}$	ϕ	$\phi_{ extstyle grout} \phi V_{ extstyle Sa} ext{ (lb)}$	
4780	1.0	0.65	3107	

9. Concrete Breakout Strength of Anchor in Shear (Sec. 17.5.2)

Shear perpendicular to edge in y-direction:

 $V_{by} = \min |7(I_e/d_a)^{0.2} \sqrt{d_a \lambda_a} \sqrt{f'_c c_{a1}^{1.5}}; 9\lambda_a \sqrt{f'_c c_{a1}^{1.5}}|$ (Eq. 17.5.2.2a & Eq. 17.5.2.2b)

<i>l</i> e (in)	da (in)	λ_a	f'c (psi)	Ca1 (in)	V_{by} (lb)			
2.04	0.375	1.00	3000	7.72	7067			
$\phi V_{cbgy} = \phi (A$	$_{Vc}/A_{Vco})\Psi_{ec,V}\Psi_{ec}$	$_{\text{ed,V}} arPsi_{ ext{c,V}} arPsi_{ ext{h,V}} V_{ ext{by}}$	(Sec. 17.3.1 & E	q. 17.5.2.1b)				
A_{Vc} (in ²)	A_{Vco} (in ²)	$\Psi_{ec,V}$	$\mathscr{V}_{ed,V}$	$\Psi_{c,V}$	$\Psi_{h,V}$	V_{by} (lb)	ϕ	ϕV_{cbgy} (lb)
134.40	268.19	1.000	1.000	1.400	1.522	7067	0.70	5282



Company:	Waypoint Engineering	Date:	9/5/2018
Engineer:	JF	Page:	5/5
Project:	Stainless Cable Solutions Concrete	e Anchor	age
Address:	601 Main Street #400		
Phone:	360.635.6611		•
E-mail:	jared@waypointwa.com		

10. Concrete Pryout Strength of Anchor in Shear (Sec. 17.5.3)

 $\phi V_{cpg} = \phi k_{cp} N_{cbg} = \phi k_{cp} (A_{Nc}/A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \text{ (Sec. 17.3.1 \& Eq. 17.5.3.1b)}$

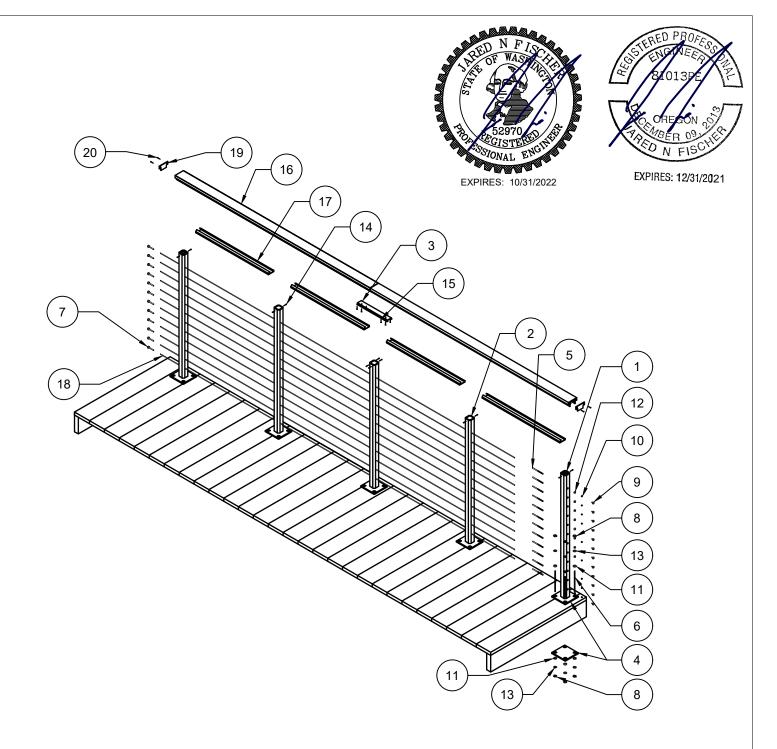
Kcp	A_{Nc} (in ²)	A_{Nco} (in ²)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$arPsi_{cp,N}$	N_b (lb)	ϕ	ϕV_{cpg} (lb)
1.0	96.83	37.45	1.000	1.000	1.000	0.727	3830	0.70	5041

11. Results

Interaction of Tensile and Shear Forces (Sec. 17.6.)

Tension	Factored Load, Nua	(lb) Design S	trength, øNn (lb)	Ratio	Status
Steel	1355	9133		0.15	Pass
Concrete breakout	2710	2911		0.93	Pass (Governs)
Shear	Factored Load, V _{ua}	(lb) Design S	trength, øVո (lb)	Ratio	Status
Steel	63	3107		0.02	Pass
T Concrete breakout y-	- 250	5282		0.05	Pass
Pryout	250	5041		0.05	Pass (Governs)
Interaction check N	ua/φNn Vo	ua∕φ V n	Combined Ratio	Permissible	Status
Sec. 17.61 0.	93 0.	00	93.1%	1.0	Pass

3/8"Ø SS Titen HD, hnom:3.25" (83mm) meets the selected design criteria.



NOTE:
1. REFERENCE S2.01 FOR ITEM, P/N, AND PART NAMES SHOWN HERE.





UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015	
2. TOLERANCES:	MATERIAL:	TITLE:	
x = 0.1		ISOMETRIC RAILING ASSEMBLY VIEW	
x.x = 0.1	FINISH:		
x.xx = 0.01 x.xxx = 0.001	FINISH.		
		REVISIONS: SHEET NO.:	
	DRAWN:	S1.00	
	PM: JF		

ITEM	P/N	PART NAME
1	TP100	41" TERMINATION POST
2	IP100	41" INTERMEDIATE POST
3	SP100	SPLICE PLATE
4	BP100	BASE PLATE
5	TTMS249	THREADED TENSIONING TERMINAL OR TURNBUCKLE
6	TR375	THREADED ROD, SS, 3/8
7	BT249	BUTTON TERMINAL
8	SSN375	HEX NUT, SS, 3/8
9	ACN25	ACORN NUT, SS, 1/4
10	SSN25	HEX NUT, SS, 1/4
11	SCW100	STAINLESS CAP WASHER
12	SSW25	STAINLESS WASHER
13	LBLW38	LOCK WASHER, SS, 3/8
14	SDS100	#10 x 5/8" SS18-8 SELF DRILLING PAN HEAD SCREW
15	SDS100	#10 x 5/8" SS18-8 SELF DRILLING PAN HEAD SCREW
16	TR100	TOP RAIL
17	FI100	FLAT INFILL
18	WIRE ROPE	1/8", 3/16", OR 1/4" DIA.
19	EC100	END CAP
20	ECS100 X2	#6 x 3/4 316 SS END CAP SCREW



EXPIRES: 12/31/2021



EXPIRES: 10/31/2022

NOTES:

- 1. REFERENCE S2.00 FOR ISOMETRIC PART ASSEMBLY DRAWING.
- 2. THIS DRAWING IS PROPERTY OF STAINLESS CABLE SOLUTIONS, LLC. AND IS SUBMITTED IN CONFIDENCE FOR USE IN CONNECTION WITH AN EXISTING, PENDING, OR FUTURE TRANSACTION BETWEEN US. THIS MATERIAL SHALL NOT BE REPRODUCED OR PUBLISHED IN ANY FORM OR DISCLOSED TO ANYONE OUTSIDE YOUR EMPLOY WITHOUT PRIOR WRITTEN CONSENT OF STAINLESS CABLE SOLUTIONS, LLC. THE SUBMISSION OF THIS DRAWING IS NOT INTENDED TO CONSTITUTE PUBLICATION OF SAME.
- 3. PACKAGING REQUIRED WHICH WILL AFFORD ADEQUATE PROTECTION AGAINST PHYSICAL DAMAGE DURING HANDLING, SHIPMENT, AND STORAGE.
- 4. DEBURR AND BREAK ALL SHARP EDGES.
- 5. ALL HARDWARE, INCLUDING NUTS, LAG SCREWS, HANGERS, ETC., SHALL BE GALVANIZED OR STAINLESS STEEL.

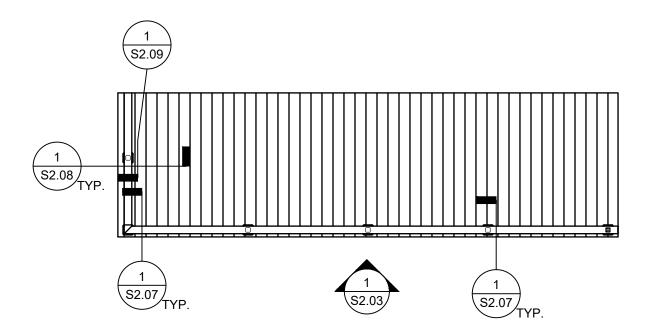


UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015	
2. TOLERANCES:	MATERIAL:	TITLE:	
x = 0.1 x.x = 0.1		ITEM, PIN, AND PART NAMES	
x.xx = 0.01 x.xxx = 0.001	FINISH:	PART NAIVIES	
X.XXX — 0.001		REVISIONS: SHEET NO.:	
	DRAWN: PM: JF	S1.01	





EXPIRES: 12/31/2021



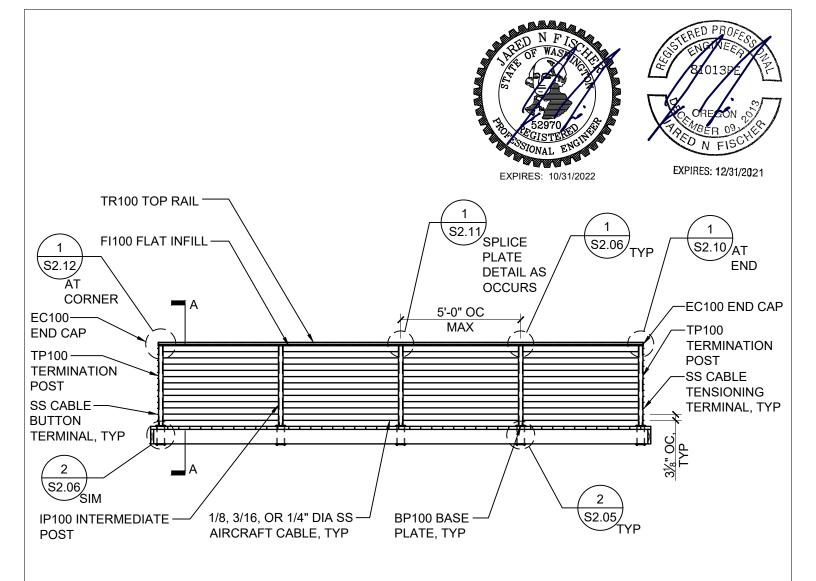
NOTE:

1. REFERENCE S2.03 FOR ELEVATION.



<u>SCS</u>			
Stainless Cable Solutions			

UNLESS NOTED OTHERWISE:	20184		BLE SOLUTIONS, LLC. SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		MAS, OR 97015	
2. TOLERANCES:	MATERIAL:	TITLE:		
x = 0.1		RAILING AND		
x.x = 0.1 x.xx = 0.01	FINISH:	DEC	K PLAN	
x.xxx = 0.001		REVISIONS:	SHEET NO.:	
	DRAWN:	1	S1.02	
	PM· JF			



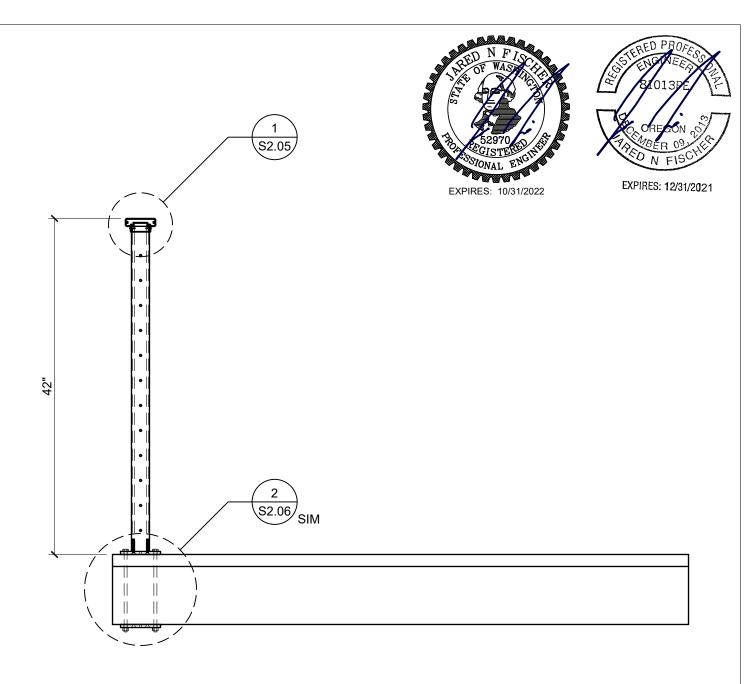
NOTE:

1. REFERENCE S2.02 FOR PLAN.



	505
Stain	less Cable Solutions

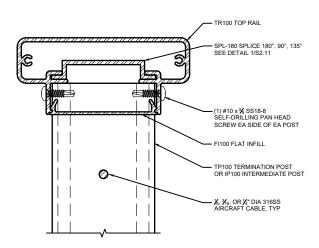
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184		LE SOLUTIONS, LLC. SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		MAS, OR 97015
2. TOLERANCES:	MATERIAL:	TITLE:	
x = 0.1		RAILING	AND DECK
x.x = 0.1		ELEVATION	
x.xx = 0.01	FINISH:		
x.xxx = 0.001		REVISIONS:	SHEET NO.:
	DRAWN:		S1.03
	PM: JF		

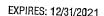






UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE		
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015		
2. TOLERANCES:	MATERIAL:	TITLE: 42" ALUMINUM		
x = 0.1 x.x = 0.1		DECK MOUNT		
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASSEMBLY		
		REVISIONS: SHEET NO.:		
	DRAWN: PM: JF	S1.04		

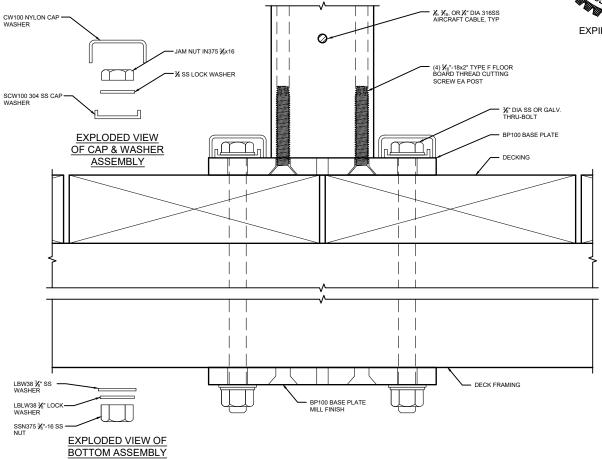




PED N FISC



TOP RAIL CONNECTION DETAIL AT TERMINATION & INTERMEDIATE POST

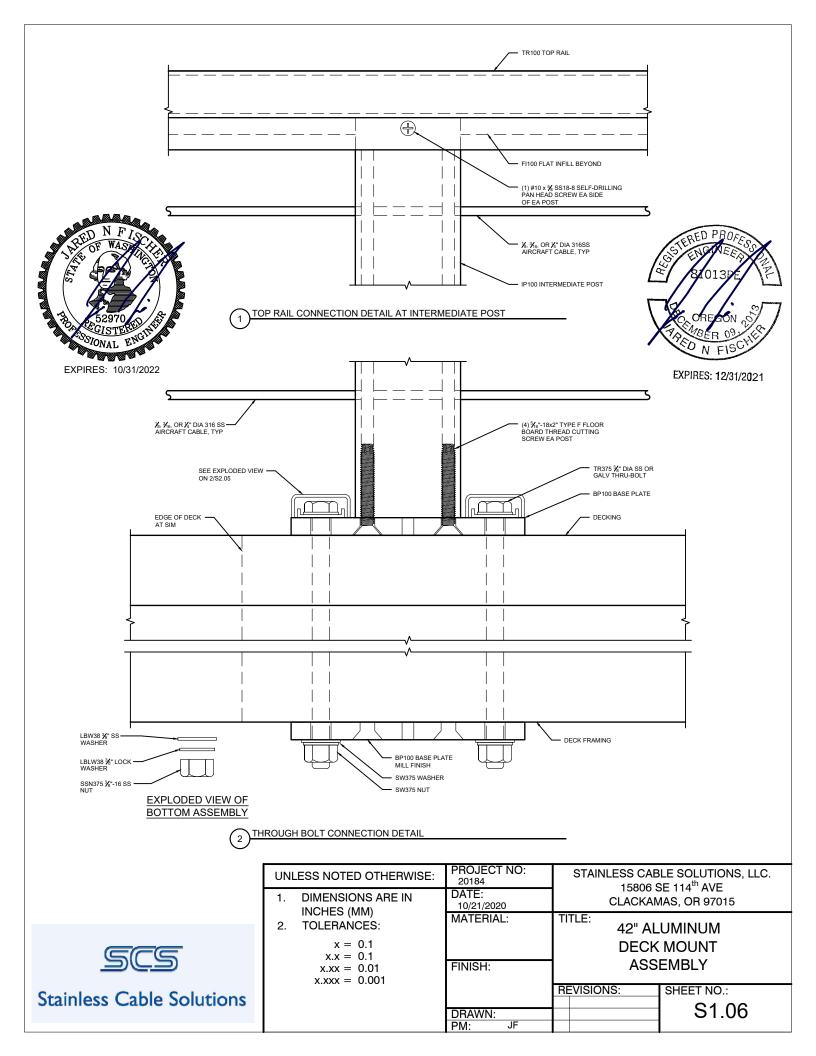


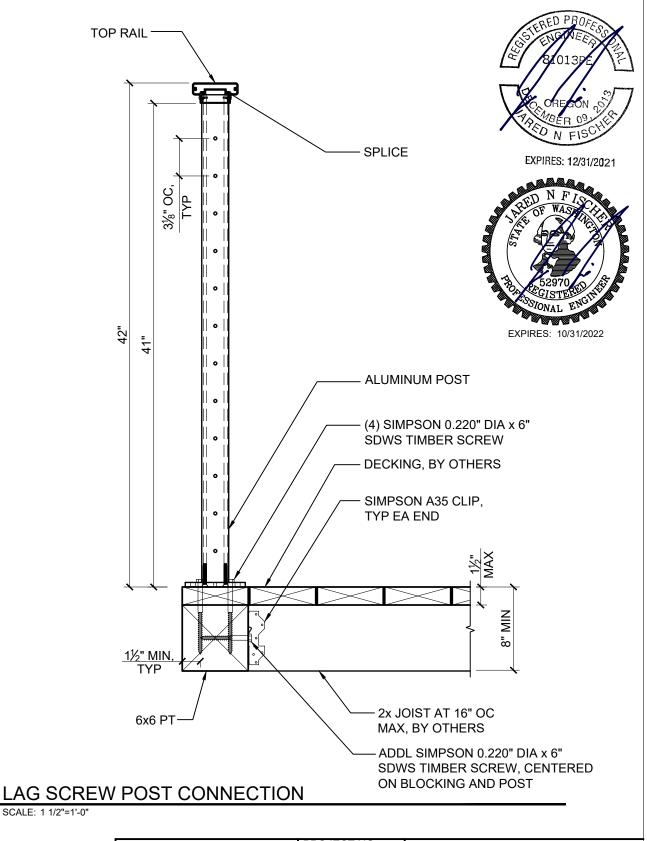
THROUGH BOLT CONNECTION DETAIL



UNLESS NOTED OTHERWISE:	20184		BLE SOLUTIONS, LLC. SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		MAS, OR 97015	
2. TOLERANCES:	MATERIAL:	TITLE: 42" ALUMINUM		
x = 0.1 x.x = 0.1		DECK MOUNT ASSEMBLY		
x.xx = 0.01 x.xxx = 0.001	FINISH:			
		REVISIONS:	SHEET NO.:	
	DRAWN:		S1.05	
	PM: JF			

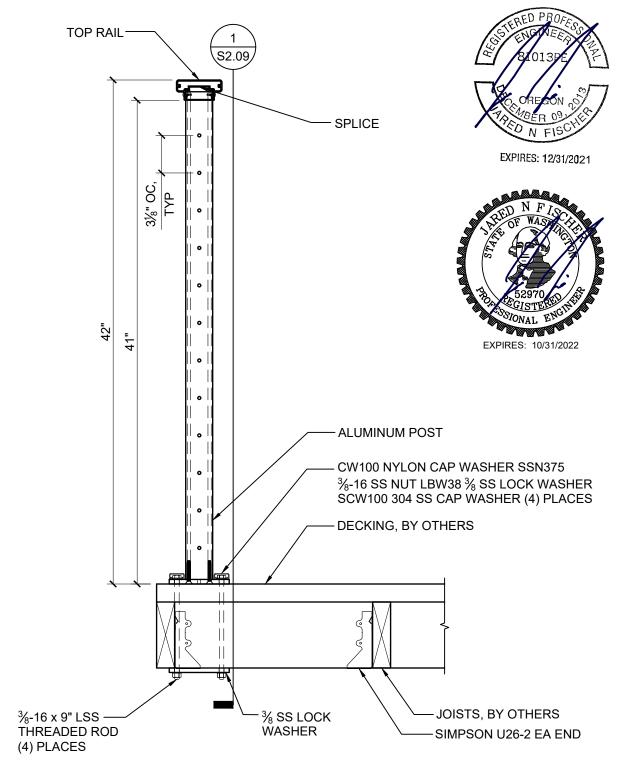
DDO IECT NO:







UNLESS NOTED OTHERWISE:	PROJECT NO: 20184		LE SOLUTIONS, LLC. SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	ATE: CLACKAMAS, OR 97015 ATERIAL: 42" ALUMINUM DECK MOUNT	
2. TOLERANCES:	MATERIAL:		
x = 0.1 x.x = 0.1			
x.xx = 0.01 x.xxx = 0.001	FINISH:		
		REVISIONS:	SHEET NO.:
	DRAWN: PM: JF		S1.07

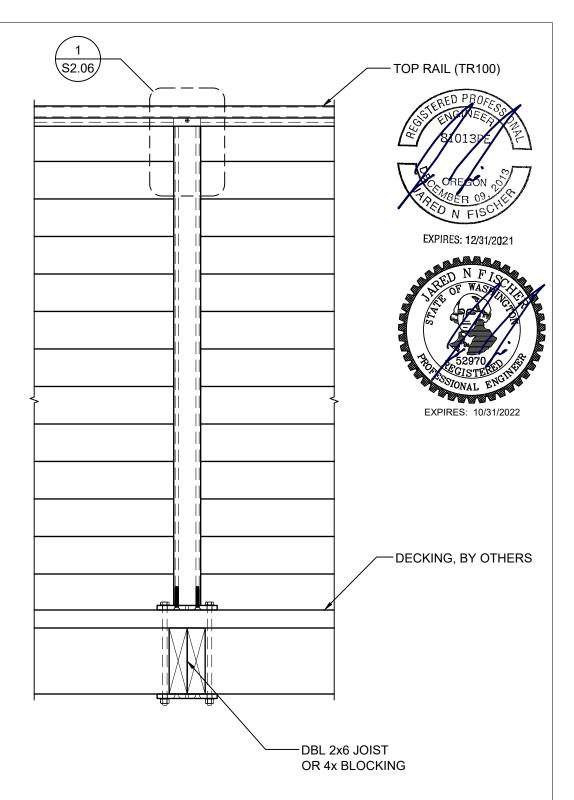


THROUGH BOLT POST CONNECTION

SCALE: 1 1/2"=1'-0"



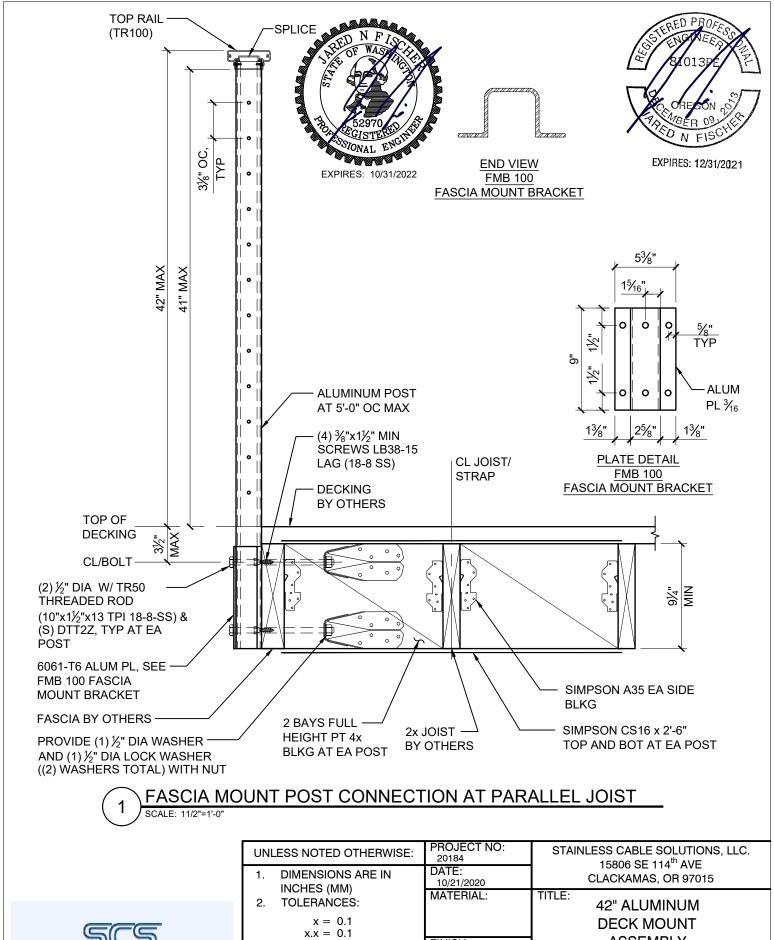
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184		LE SOLUTIONS, LLC. SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		1AS, OR 97015
2. TOLERANCES:	MATERIAL:	TITLE: 42" AL	UMINUM
x = 0.1 x.x = 0.1			MOUNT
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASSI	EMBLY
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		REVISIONS:	SHEET NO.:
	DRAWN:		S1.08
	PM: JF		



1 INTERMEDIATE POST THROUGH BOLT CONNECTION SCALE: 1 1/2"=1'-0"

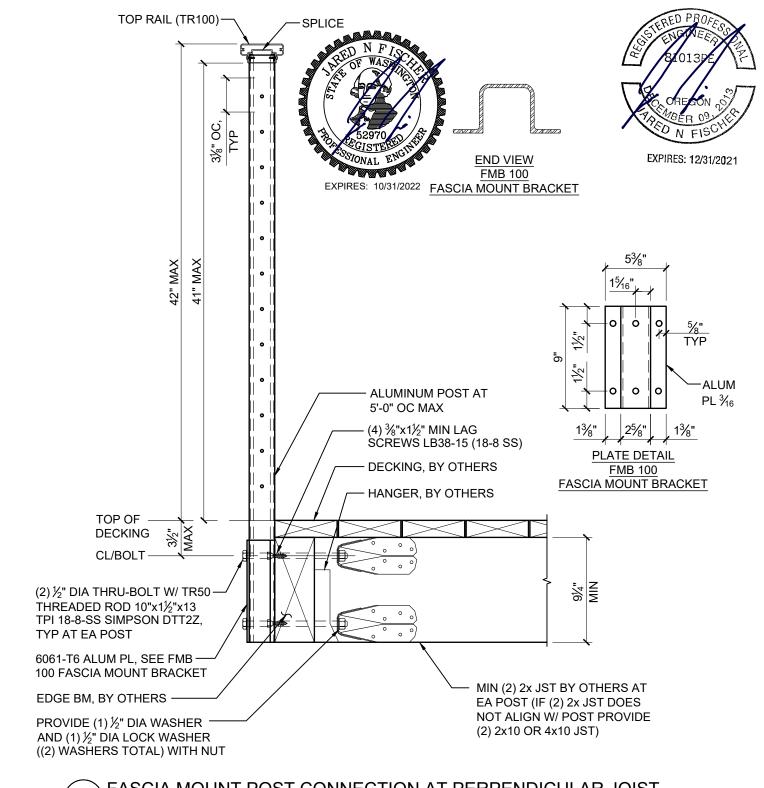


UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		1AS, OR 97015
2. TOLERANCES:	MATERIAL:	TITLE: 42" AL	UMINUM
x = 0.1 x.x = 0.1			MOUNT
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASSEMBLY	
		REVISIONS:	SHEET NO.:
	DRAWN:		S1.09
	PM: JF		





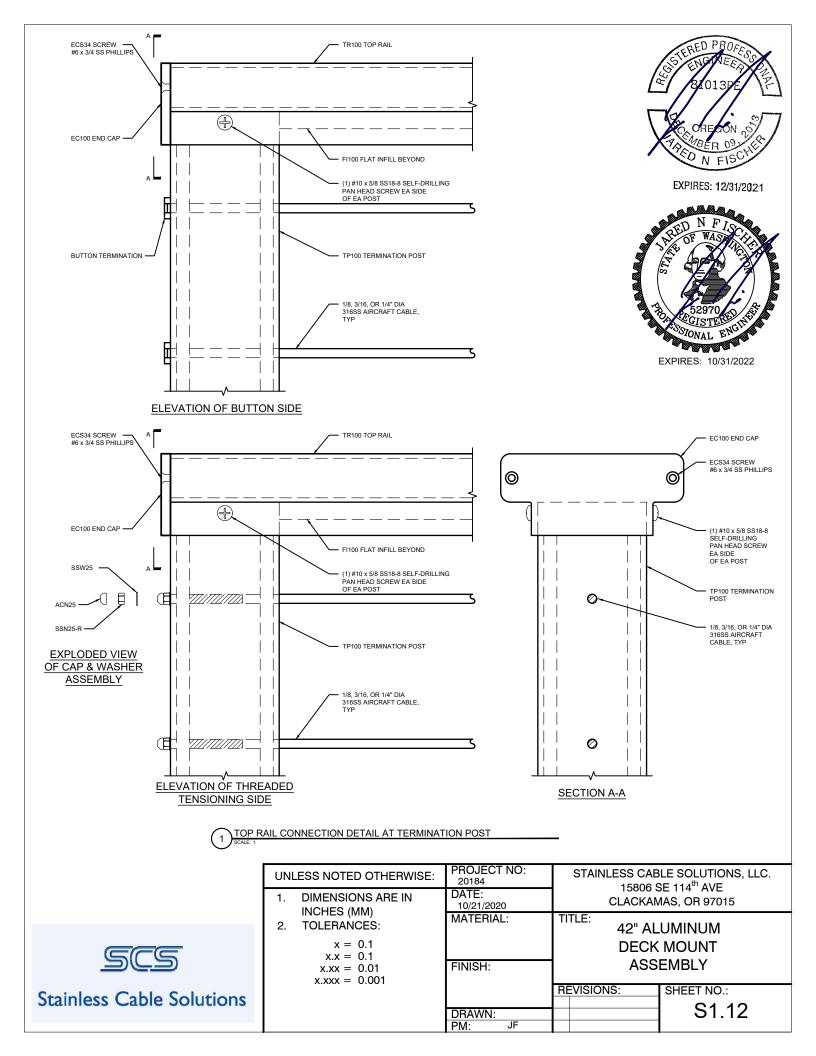
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		MAS, OR 97015
2. TOLERANCES:	MATERIAL:	TITLE: 42" AL	UMINUM
x = 0.1 x.x = 0.1			MOUNT
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASS	EMBLY
		REVISIONS:	SHEET NO.:
	DRAWN: PM: JF		S1.10

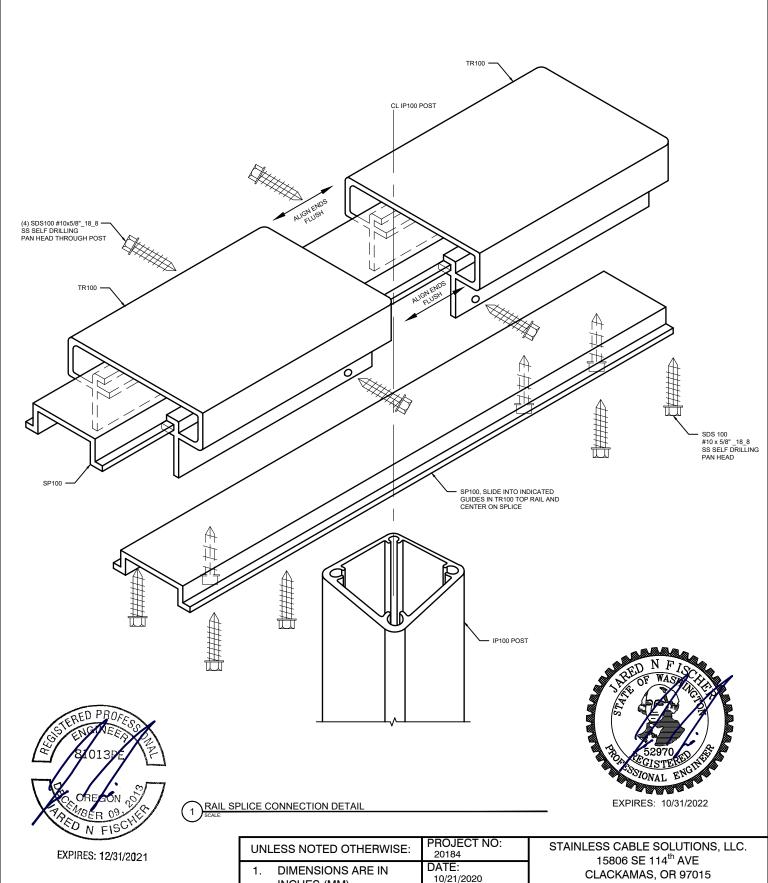


1 FASCIA MOUNT POST CONNECTION AT PERPENDICULAR JOIST SCALE: 11/2"=1'-0"



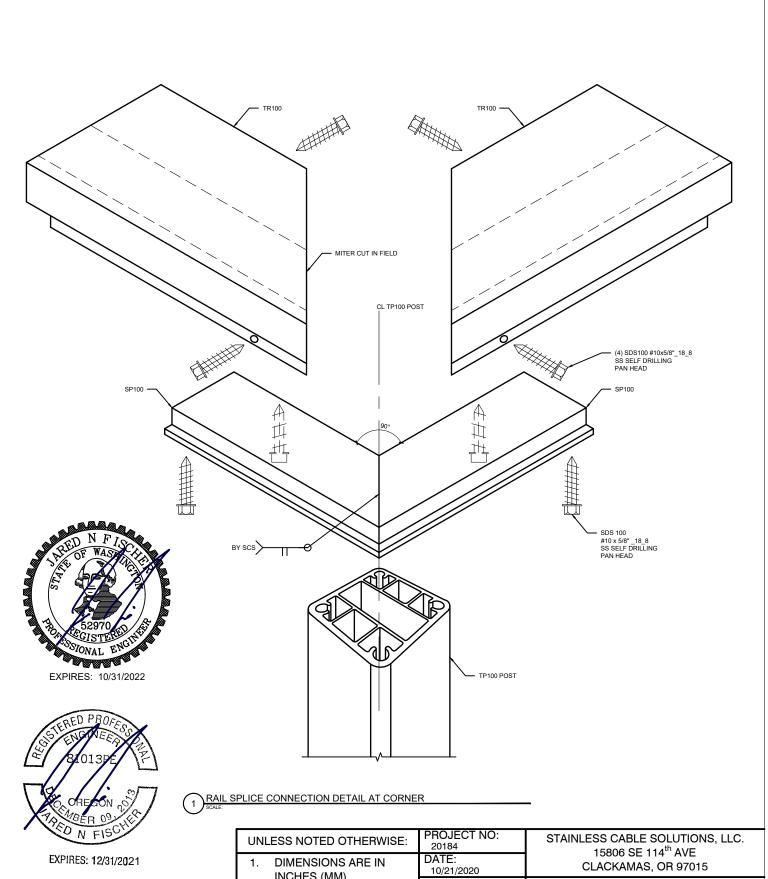
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015	
2. TOLERANCES:	MATERIAL:	TITLE: 42" ALUMINUM	
x = 0.1 x.x = 0.1		DECK MOUNT	
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASSEMBLY	
		REVISIONS: SHEET NO.:	
	DRAWN:	S1.11	
	PM: JF		







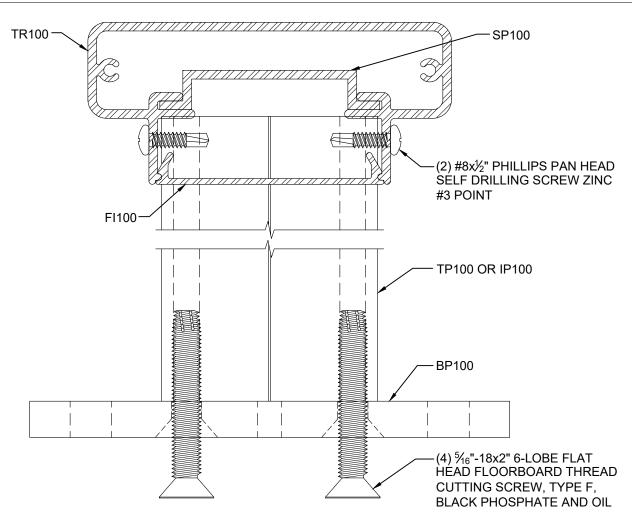
UNLESS NOTED OTHERWISE:	20184	15806 SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015	
2. TOLERANCES:	MATERIAL:	TITLE: 42" ALUMINUM	
x = 0.1 x.x = 0.1		DECK MOUNT	
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASSEMBLY	
		REVISIONS: SHEET NO.:	
	DRAWN:	S1.13	
	PM: JF		



SCS

Stainless Cable Solutions

UNLESS NOTED OTHERWISE:	20184	15806 SE 114 th AVE CLACKAMAS, OR 97015 TITLE: 42" ALUMINUM	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		
2. TOLERANCES:	MATERIAL:		
x = 0.1 x.x = 0.1			MOUNT
x.xx = 0.01 x.xxx = 0.001	FINISH:	ASS	EMBLY
		REVISIONS:	SHEET NO.:
	DRAWN:		S1.14
	PM: JF		O 1. 1 -1



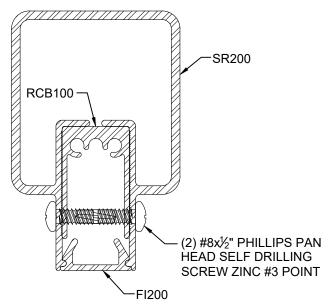


EXPIRES: 12/31/2021

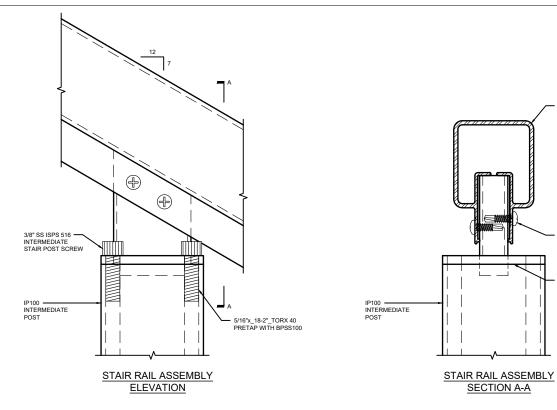


EXPIRES: 10/31/2022

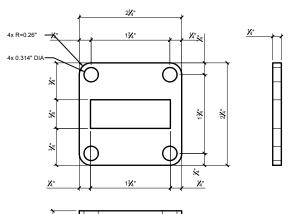


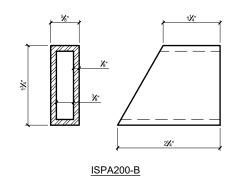


UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE CLACKAMAS, OR 97015			
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020				
2. TOLERANCES:	MATERIAL:	TITLE:			
x = 0.1 x.x = 0.1		RAIL ASSEMBLY	DIAGRAMS		
x.xx = 0.01 x.xxx = 0.001	FINISH:				
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		REVISIONS: SHE	EET NO.:		
	DRAWN: PM: JF		S1.15		



TOP STAIR RAIL CONNECTION DETAIL

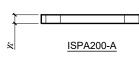


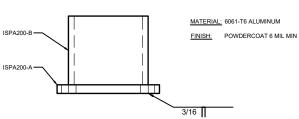


SR200 STAIR RAIL

(2) #10 x 5/8 SS18-8 SELF-DRILLING PAN HEAD SCREW EACH SIDE

SPC100 STAIR POST CAP







STAIR POST CAP (ISPA200) **ASSEMBLY**

2 INTERMEDIATE STAIR POST ADAPTER

EXPIRES: 12/31/2021



SSIONAL ENGINE

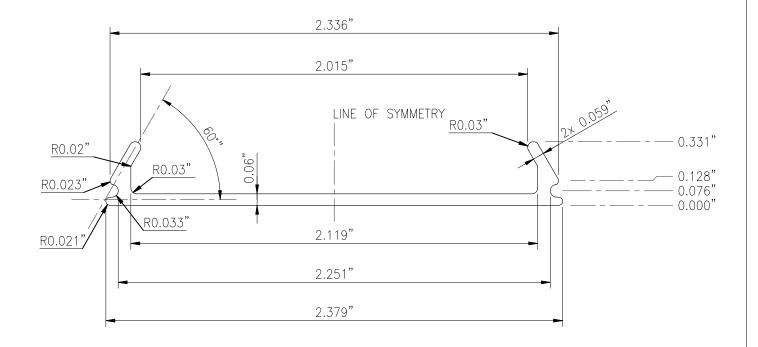
EXPIRES: 10/31/2022

UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE CLACKAMAS, OR 97015				
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020					
2. TOLERANCES: x = 0.1 x.x = 0.1 x.xx = 0.01 x.xx = 0.001	MATERIAL: FINISH:	STAIR RAIL ASSEMBLY				
	DRAWN: PM: JF	REVISIONS:	SHEET NO.: \$1.16			





EXPIRES: 12/31/2021





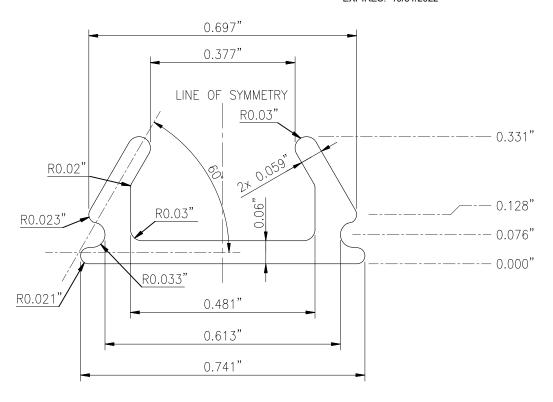


UN	LESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC 15806 SE 114 th AVE	
1.	DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		MAS, OR 97015
2.	TOLERANCES:	MATERIAL: 6063T5	TITLE:	
	x = 0.1 x.x = 0.1	ALUMINIUM LENGTH = 15'-0"		T INFILL 1100
	x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT	·	1100
		6 MIL MIN	REVISIONS:	SHEET NO.:
3.	SCALE: 2:1	DRAWN: PM: JF		S2.01





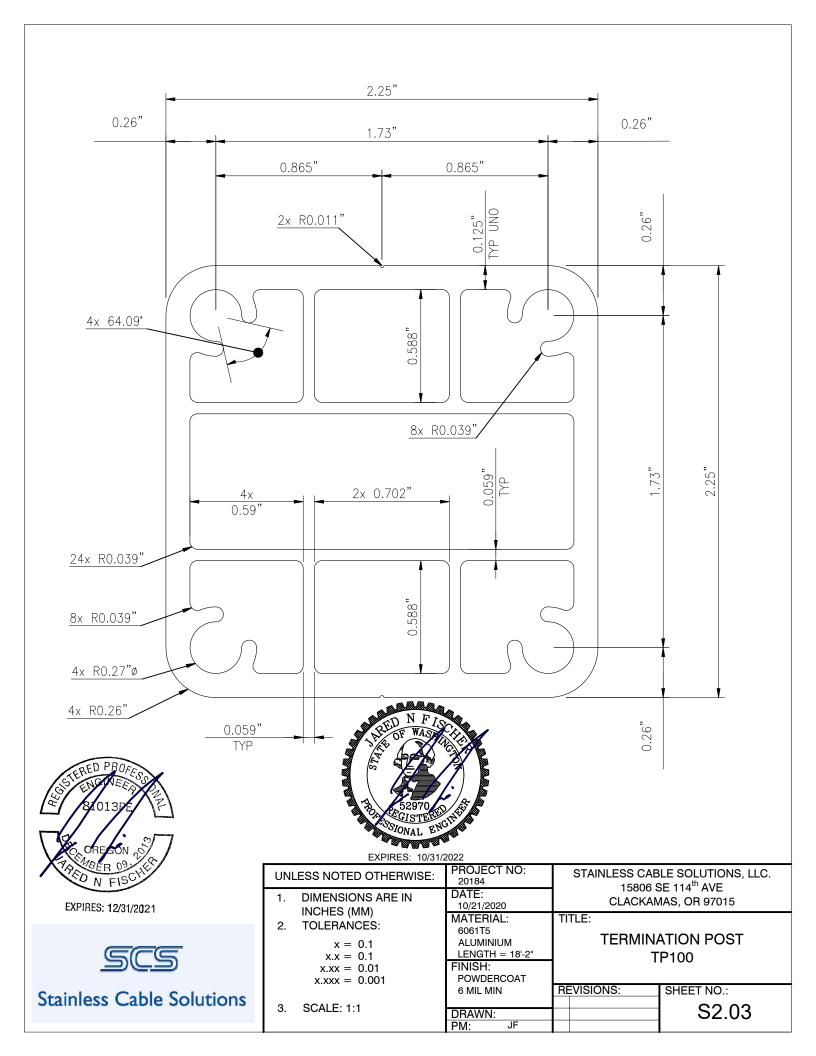
EXPIRES: 10/31/2022 EXPIRES: 12/31/2021

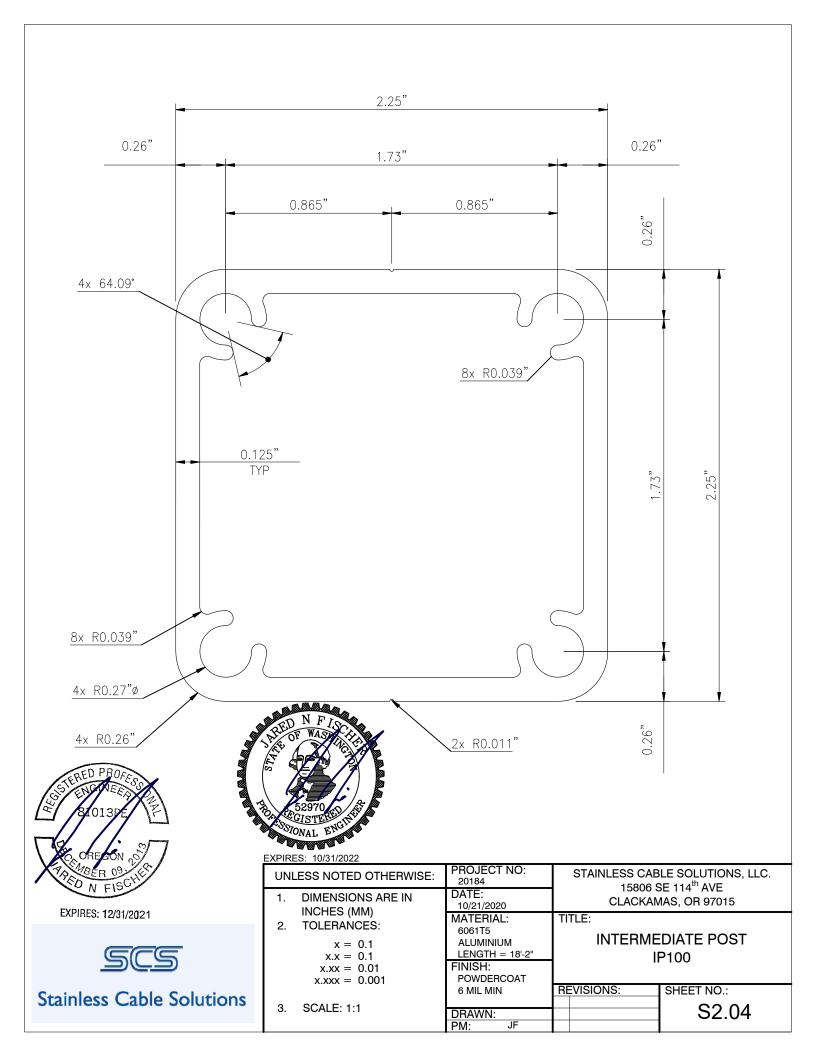




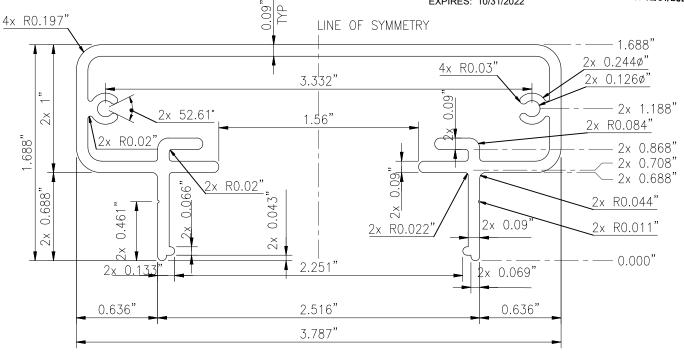


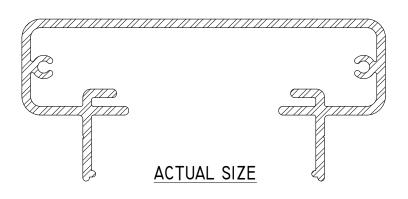
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184		SLE SOLUTIONS, LLC. SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015	
2. TOLERANCES:	MATERIAL: 6063T5	TITLE:	
x = 0.1 x.x = 0.1	ALUMINIUM LENGTH = 15'-0"	STAIR FLAT INFILL Fl200	
x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT		
1	6 MIL MIN	REVISIONS:	SHEET NO.:
3. SCALE: 4:1	DRAWN: PM: JF		S2.02





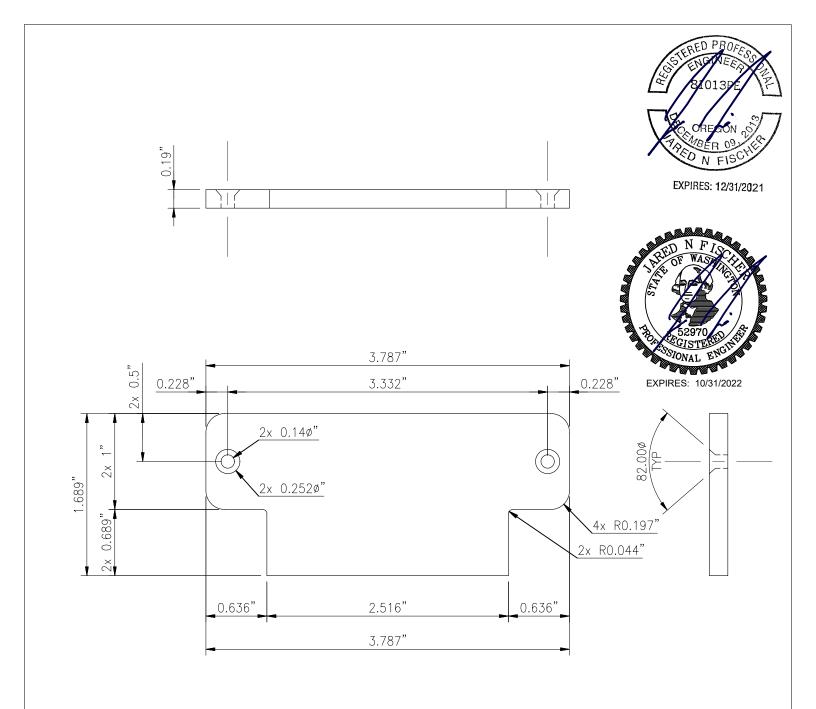






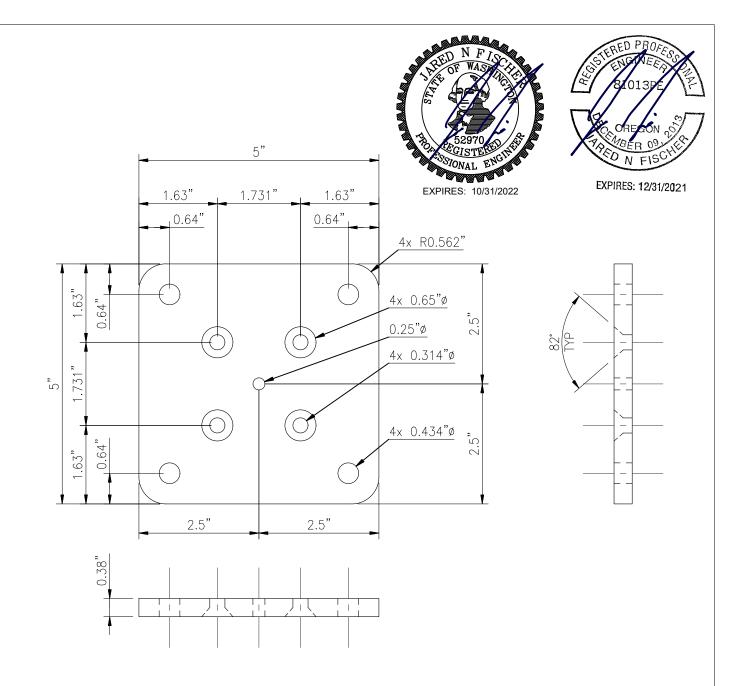
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE CLACKAMAS, OR 97015	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		
2. TOLERANCES:	MATERIAL: 6061T5	TITLE:	D DAII
x = 0.1 x.x = 0.1	ALUMINIUM LENGTH = 18'-2"	TOP RAIL TR100	
x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT	'	11100
X.XXX — 0.001	6 MIL MIN	REVISIONS:	SHEET NO.:
3. SCALE: 2:1	DRAWN: PM: JF		S2.05





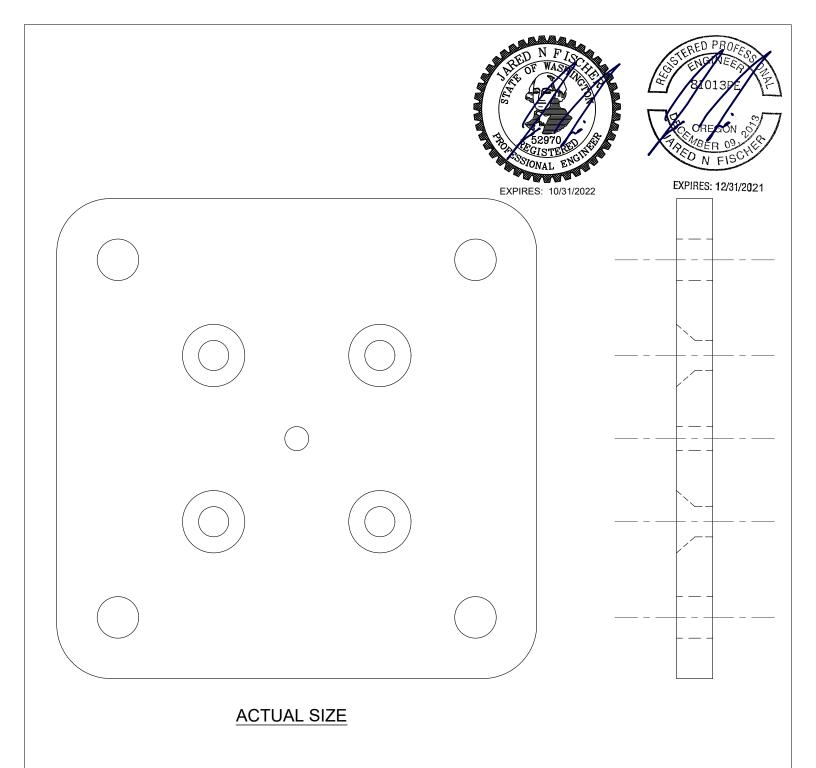


UNLESS NOTED OTHERWISE:	PROJECT NO: 20184		SLE SOLUTIONS, LLC. SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015	
2. TOLERANCES:	MATERIAL: 60631T5	TITLE:	D 04B
x = 0.1 x.x = 0.1	ALUMINIUM	END CAP EC100	
x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT	_	0100
1	6 MIL MIN	REVISIONS:	SHEET NO.:
3. SCALE: 1:1	DRAWN: PM: JF		S2.06





UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC 15806 SE 114 th AVE CLACKAMAS, OR 97015		STAINLESS CABLE SOLUTIONS, LLC.	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020				
2. TOLERANCES: x = 0.1 x.x = 0.1	MATERIAL: 6061T5 ALUMINIUM	BASE PLATE BP100			
x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT 6 MIL MIN	REVISIONS:	SHEET NO.:		
3. SCALE: 1:2	DRAWN:		S2.07		



 $\frac{\text{NOTE:}}{\text{REF SHEET S7 FOR DIMENSIONS}}$

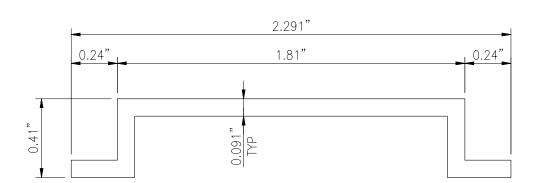


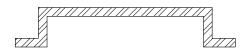
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC 15806 SE 114 th AVE CLACKAMAS, OR 97015	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		
2. TOLERANCES:	MATERIAL: 6061T5	TITLE:	
x = 0.1 x.x = 0.1	ALUMINIUM	BASE PLATE BP100	
x.x = 0.1 x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT	۱ ۲	100
X.XXX = 0.001	6 MIL MIN	REVISIONS:	SHEET NO.:
3. SCALE: 1:1	DRAWN: PM: JF		S2.08





EXPIRES: 10/31/2022 EXPIRES: 12/31/2021





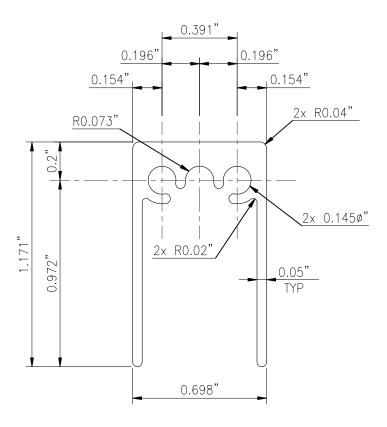
<u>5C5</u>
Stainless Cable Solutions

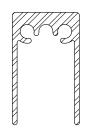
9
(





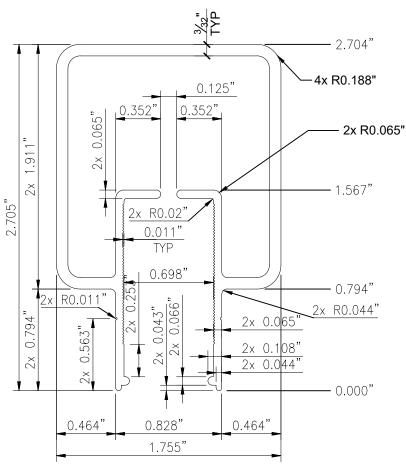
EXPIRES: 10/31/2022 EXPIRES: 12/31/2021





SCS		
Stainless Cable Solutions		

UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015
2. TOLERANCES:	MATERIAL: 6063T5	TITLE:
x = 0.1 x.x = 0.1	ALUMINIUM LENGTH = 12'-0"	RAIL CONNECTING BLOCK RCB100
x.xx = 0.01 x.xxx = 0.001	FINISH: NONE	1100100
1		REVISIONS: SHEET NO.:
3. SCALE: 2:1	DRAWN: PM: JF	S2.10

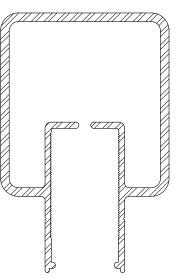




EXPIRES: 12/31/2021



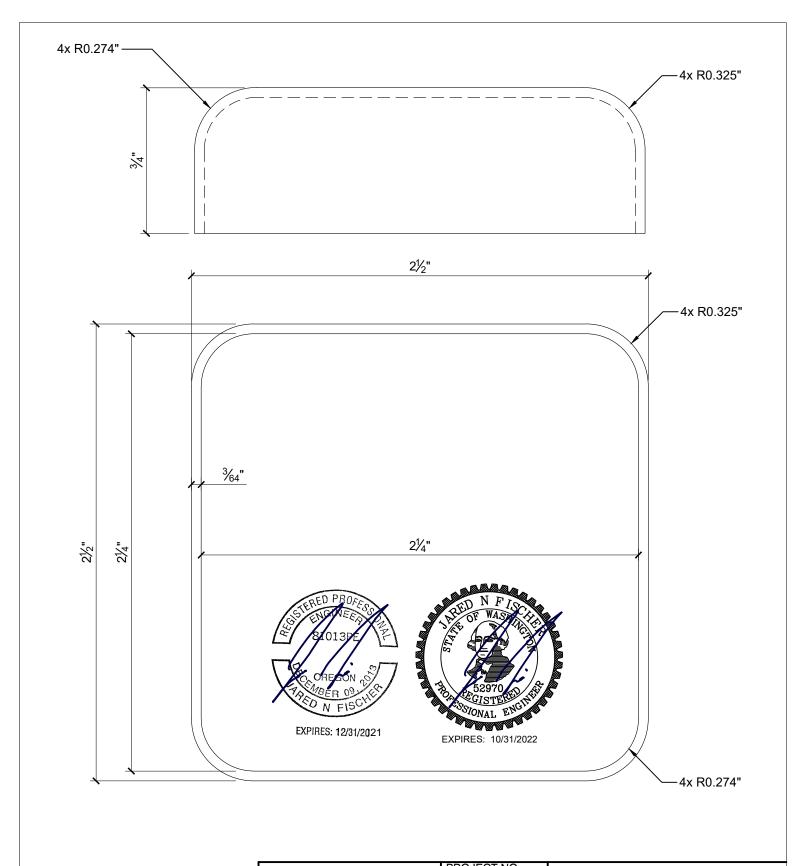
EXPIRES: 10/31/2022



ACTUAL SIZE

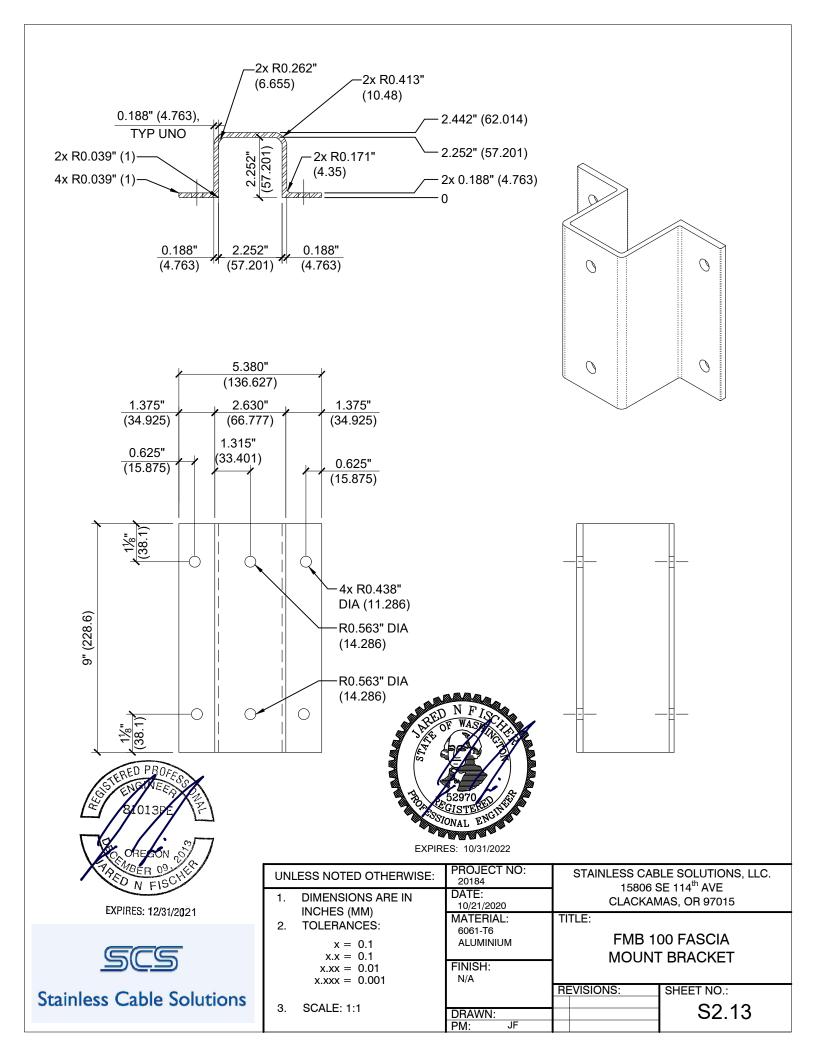
505			
Stainless Cable Solutions			

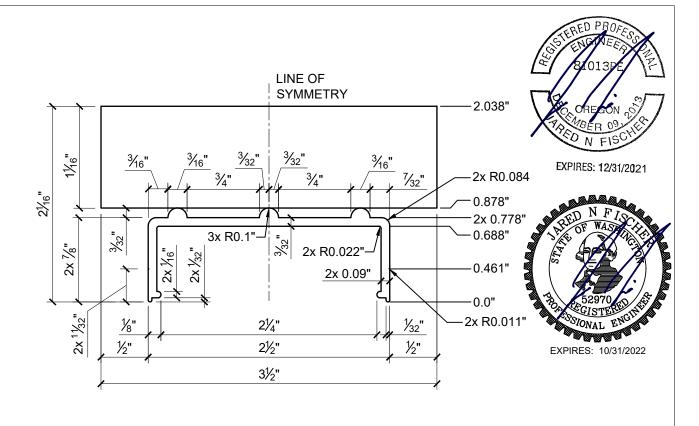
UNLESS NOTED OTHERWISE:	PROJECT NO: 20184		SLE SOLUTIONS, LLC.
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		SE 114 th AVE MAS, OR 97015
INCHES (MM) 2. TOLERANCES: x = 0.1 x.x = 0.1 x.xx = 0.01 x.xx = 0.001	MATERIAL: 6061T5 ALUMINIUM LENGTH = 18'-2" FINISH: POWDERCOAT	STAIR RAIL SR200	
3. SCALE: 2:1	6 MIL MIN DRAWN: PM: JF	REVISIONS:	SHEET NO.: S2.11

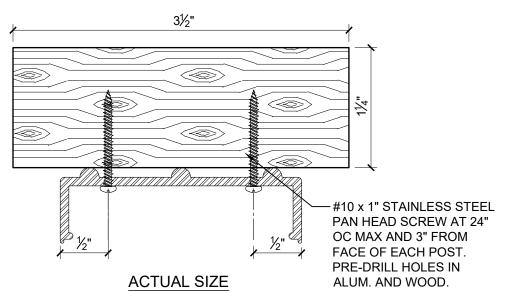




UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC 15806 SE 114 th AVE	
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020		MAS, OR 97015
2. TOLERANCES:	MATERIAL: A1050	TITLE:	OT 0 4 D
x = 0.1 x.x = 0.1	ALUMINIUM		ST CAP C100
x.xx = 0.01 x.xxx = 0.001	FINISH: POWDERCOAT] '	0100
	6 MIL MIN	REVISIONS:	SHEET NO.:
3. SCALE: 1:1	DRAWN: PM: JF		S2.12

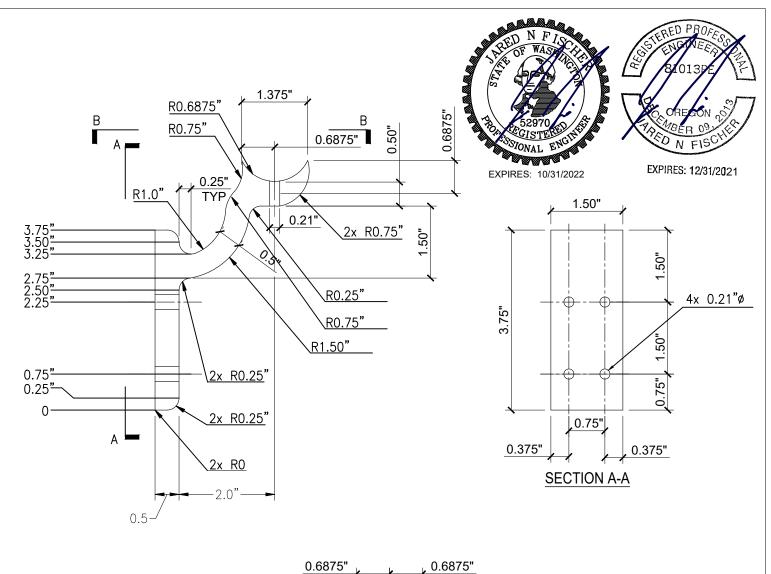


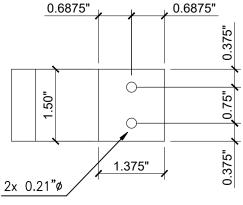






UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015
2. TOLERANCES:	MATERIAL:	TITLE:
x = 0.1 x.x = 0.1		
x.xx = 0.01 x.xxx = 0.001	FINISH:	
		REVISIONS: SHEET NO.:
3. SCALE: 1:1	DRAWN:	S2.14

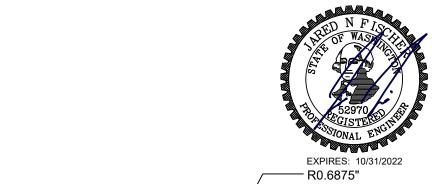




SECTION B-B

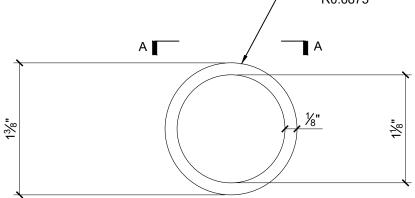


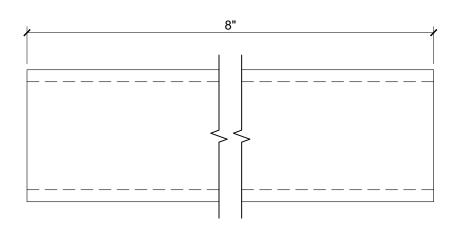
	UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC. 15806 SE 114 th AVE
	DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015
	2. TOLERANCES:	MATERIAL: 6061-T6	TITLE:
	x = 0.1 x.x = 0.1 x.xx = 0.01 x.xxx = 0.001	ALUMINIUM	ADA HAND RAIL BRACKET HRB 20
		FINISH: N/A	BIVIORET TIMB 20
			REVISIONS: SHEET NO.:
	3. SCALE: 1:1	DRAWN: PM: JF	S2.15





EXPIRES: 12/31/2021





SECTION A-A



UNLESS NOTED OTHERWISE:	PROJECT NO: 20184	STAINLESS CABLE SOLUTIONS, LLC 15806 SE 114 th AVE
DIMENSIONS ARE IN INCHES (MM)	DATE: 10/21/2020	CLACKAMAS, OR 97015
INCHES (MM) 2. TOLERANCES: x = 0.1 x.x = 0.1	MATERIAL: N/A	TITLE: ITEM NUMBER: ADA_GR_MF PART NUMBER: ADA GRAB
x.xx = 0.01 x.xxx = 0.001	FINISH: N/A	RAIL_MILL FINISH REVISIONS: SHEET NO.:
3. SCALE: 1:1	DRAWN: PM: JF	S2.16